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A HANDY PLATELAYER'S GUIDE.

TABLES AND DIAGRAMS

OF

SWITCHES & CROSSINGS:

A HANDY

PLATELAYER'S GUIDE.

BY

THOMAS SUMMERSON & SONS,

ALBERT HILL FOUNDRY,

DARLINGTON.

THIRD EDITION.

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PREFACE.

T is sixteen years since the first edition of these tables was published by us. A second edition, enlarged and revised, appeared in 1885, and we now offer a third edition revised and further enlarged. Owing to the addition of extra tables and more matter, we have reluctantly been obliged to depart from the original handy form of simply two boards printed on the inside, by which the whole of the tables were presented to view at once, but we trust that the value of the added information and data will be found some compensation for the book form in which this addition appears. Our main object in these tables is to assist the platelayer when putting in sidings, by providing him with the distances, which too often he is left to work out empirically at the cost of much unnecessary labour.

We have also had in view the providing of a handy book of ready reference for engineers engaged in planning new sidings, where they will find useful data in a concise form.

In deference to numerous applications we have in this addition included tables referring to other eight gauges besides the 4 ft. $8\frac{1}{2}$ in., viz., the 1 ft. 6 in., 2 ft., 2 ft. 6 in., 3 ft., 3 ft. $3\frac{3}{8}$ in. or metre, 3 ft. 6 in., 5 ft. 3 in., and 5 ft. 6 in.

The alteration in the distances, contained in this edition of the tables, as compared with the previous one is due to our having taken inside or gauge dimensions as a basis instead of using centre lines as heretofore.

We shall always be glad to receive suggestions with a view to making future editions of these tables more useful, and we trust that the present one will meet with the same favour as its predecessors.

Albert Hill Foundry,

Darlington, June 26th, 1895.

GENERAL INFORMATION.

Gauge. The gauge of a railway is always measured inside and inside of the rails. The standard gauge, not only in this country, but on the Continent and in the United States, is 4 ft. $8\frac{1}{2}$ in., the Irish gauge is 5 ft. 3 in., and in India there are two gauges, viz., the metre (3 ft. $3\frac{3}{8}$ in.), and the 5 ft. 6 in. gauge.

The broad gauge (7 ft.), introduced by Brunel, which at one time contested the field with the present standard, was finally abandoned a few years ago. Narrower gauges than 4 ft. 8½ in. are, however, a good deal used both in this country and abroad for light traffic, where it would not pay to put down the standard gauge.

Weight of Having determined the load per axle,
Rail. including weight of truck, the weight of
rail most suitable can be found by the formula

$$W = \sqrt{L \times 375}.$$

(Multiply the load in tons on axle by 375 and extract the square root.)

W = Weight of rail in lbs. per yard.

L = Greatest load on any axle.

This rule is based upon the sleepers being pitched 3 ft. centres. The weight of the rail, roughly, may be reduced in direct proportion for shorter pitches. As the greatest load is generally that on one of the axles of the locomotive, this may be

arrived at approximately by multiplying the extreme load on a wagon axle by two.

In the following table the gauges named are those usually adopted for the corresponding weight of rail.

	Ins.	0	0	0	9	 2,2	,	<i>ب</i>	
	F.	8	8	3	3	4	or 5		
Gauge of Road,	١.	to	:	:	2	•		•	
	Ins.	9	9	9	0	9	878		0
	F. 1		H	8	3	3	4 2		~
Approx. Cross Section of Sleepers.	Ins. Ins. 4 × 2	5 × 2 ½	6 × 3	$7 \times 3\frac{1}{2}$	$7 \times 3^{\frac{1}{2}}$	$9 \times 4^{\frac{1}{2}}$	$9 \times 4^{\frac{1}{2}}$	10 × 5	10 × 5
					sc so	හ 4			H
Approx. size of Round Chair Spikes.	Ins.	18	16	~ o1	5	•	ec 44	~ x	to
	= -	, H	,.) L	·			-414		
					:31	sc so			r 20
Size of Dog Spikes for flange rails.	Ins. × 2½	× 2 3 1	×	× 3½	× 3½	× 4½	×	× 5,1	9 ×
	Ins.	89 30	18	∟ 39	16	sc so	11	ω¦4 <u>,</u>	1 3
	Ins.	~ sq	sc ∞	uc so	හ 4		c ~		1
Approx. size of Fish Bolts.	ئ ت	:	•	•	•	j.	\$	in.	9
Po size wordqA	Ins.	es xo	⊣ 31	⊣ 37	nc xo	ω¦4. • •	හ 4	8 11	r-120
	lbs.	:	:	:	:		lbs.	:	2
Weight of Rail in lbs. Per yard, suitable for supports, 3 ft. centres.	14	20	30	9	50	lbs.	65	75	90
	2	=	:	:	:	56	5	:	:
	12	18	25	35	45		9	10	85
Greatest Load per axle, in tons.	Ton		Tons	;		:	,	:	
	-18	H	8	4	9	8	10	15	20

Curves Standard Gauge. Curves as quick as 60 ft. can be worked by a four-wheeled locomotive with a wheel base of 9 ft. 6 in., and an ordinary

truck can be screwed round a 30-ft. radius by widening the gauge, if there is no crossing to go through. With crossings, nothing less than 60 ft. should be attempted, but when laying out sidings for works, unless very much confined for space, we should fix the minimum at 120 ft. for four-wheeled locomotives with wheel base up to 9 ft. 6 in., or say twice the gauge.

In the case of sidings to be used by main line locomotives, it is necessary to make the curves in accordance with the regulations of the Railway Company to whose lines they are connected, for some companies require a minimum of 5, or even 6 chains (i.e., 330 or 396 ft.) for curves where their locomotives have to enter.

*Recent practical tests go to show that a variation of the wheel base does not have a very marked influence on the resistance, until a very long wheel base is reached, but for safe working we think it is advisable to increase the radius of a curve in direct ratio of the wheel base.

In dealing with confined spaces, where it is necessary to minimize the sweep of the curves, they might, for wagons only, at slow speeds, be reduced to a radius equal to 10 times the wheel base, and for locomotives to 12 times the wheel base, always bearing in mind that long curves are a great advantage in working traffic, not only enabling it to

[&]quot;See Article on "The Kesistance offered by Curves on Railways," in the Engineer of July 6th, 1894.

be more quickly moved, but saving considerable expense by way of wear and tear, both to the roads and the vehicles, not to mention the trouble and annoyance due to derailment, interlocking buffers, &c., contingent upon sharp curves. The shortest radius given in Table No. 1, viz.: 29 ft., is only considered practicable for light trollies or wagons with a wheel base of 3 or 4 ft. worked by hand.

The buffers of double-bolster trucks 14 to 15 ft. wheel base are apt to interlock on curves below 100 ft. radius.

Curves for other basis of calculation is 120 ft. minimum for the standard gauge, the radii for the other gauges, being as the square of the gauge for similar wheel bases, that is wheel bases in the same ratio of the gauge. The shorter radii for hand or horse traffic may also be used for locomotives travelling at slow speeds, with a wheel base not exceeding 1½ times the gauge.

As we have found a certain amount of confusion in some quarters with reference to the meaning of the term "Wheel Base," we may as well explain that it is the measurement centre and centre of the rigid wheels farthest apart, belonging to any single locomotive or vehicle. In the case of one or more swivelling bogies, each bogie may be looked upon as a separate vehicle, and when bogies are used in conjunction with rigid wheels, the wheel base is the distance from the centre of the extreme rigid wheels to midway between the centres of the wheels under the bogie.

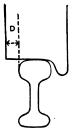
Table giving approximate minimum radii of curves suitable for wheel bases of about twice the gauge:

	auge. in.	Rad ft.				ft. in.
	6	I 2		may be red	uced for hand	
				or horse	traffic to .	. 10 0
2	0	22	0	,,	,,	15 0
2	6	34	0	,,	,,	25 O
	0	50	0	,,	,,	40 0
3	$3\frac{3}{8}$ (metre)	59	0	,,	,,	45 0
3	6	67	0	,,	,,	50 O
4	$8\frac{1}{2}$	I 20	0	,,	,,	90 O
5	3	150		,,,	,,	115 0
5	6	165	0	,,	,,	125 0

Addition to Gauge on Curves To give more freedom on sharp curves, and to prevent the road being unduly strained by the wedging action of the

wheel flanges, it is sometimes advisable to stretch the gauge a little. It is difficult to give rules for general application as to what this addition to the gauge should be, therefore a good deal must be left to the platelayer's judgment, only he should avoid widening it by more than the distance D (see Fig. 1), measured on the narrowest tyres in use.





D for the Standard Gauge runs from $\frac{7}{8}$ to 1 inch.

The following formulæ will be found useful as a basis in determining the addition to the gauge.

R = Radius of curve in feet.

G = Gauge in feet.

W = Addition to gauge in inches.

When the longest wheel base =
$$G \times 2$$
 then $W = \frac{44}{R}$
,, , = $G \times 3$,, $W = \frac{98}{R}$
., , , = $G \times 4$,, $W = \frac{180}{R}$

Where there are crossings, care must be taken to give extra flangeway clearance to the check rails on the curved side to the extent of one half of the addition that is given to the gauge; otherwise the wheels will be deprived of bearance just at the place where it is most needed, that is in the space between the knees and the nose of the crossing. With the usual flangeway clearance we would advise that in no case should the gauge be widened more than $\frac{1}{2}$ inch at the nose of crossings.

Super-elevation of the outer rail on curves.

On curves, to relieve the side presouter rail sure of the wheel flanges against the rails, due to a tendency of the train to go forward in a straight line, it is necessary to elevate the outer rail above the inner one, by packing under the sleepers. The amount of this super-elevation should be as the square of the train speed, and inversely as the radius of the curve. Where the train speed varies considerably the

super-elevation should be adjusted to the speed of the greatest weight of traffic. For slow speeds about sidings it may be dispensed with altogether. The platelayer should begin to cant the sleepers on the straight a few yards before the curve is reached, gradually attaining the full super-elevation at a point not far from the spring of the curve, and similarly letting it die out gradually into the straight at the opposite end. The values in our table* are deduced from the formula $E = \frac{V^2 \times 5}{2R}$ where 5 is a constant for the standard gauge:—

E = Super-elevation of outer rail in inches.

V = Speed of train in miles per hour.

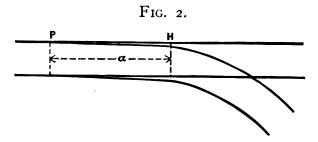
R = Radius of curve in feet.

For other gauges E varies in direct ratio, half the super-elevation being required for a 1 ft. 6 in. gauge that is necessary for a 3 ft. 0 in. one.

Where it is not convenient to elevate the outer rail, a check rail should be placed on the inside of the curve. *(See Table No. 7, giving superelevation, at end of book.)

Switches
Points. Suit the situation for which they are intended; the usual lengths for the standard gauge on main lines being 12 ft., with a proportion of 15 ft. and 18 ft., whilst about sidings the lengths run principally 9 ft., down to as low as 6 ft. The principal object in long switches is to make an easy turn off; they have also the advantage

of additional stability as compared with short ones, for, being secured only at one end, switches are liable to rock and jump when heavy loads are passing over them. The lengths of switches should in a measure be adapted to the radius of the curve, for obviously there is no advantage in making the angle at the point less than the angle at the heel. This will more readily be understood by reference to Fig. 2 below, which shows a pair of long switches (a) applied to a short curve, whereby the abruptness of the angle of turnout is met at the heel of the Switches (H) instead of the point (P).

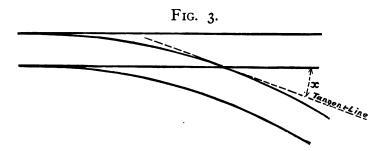


In general practice, for the standard gauge it will be found that there is nothing gained by making the switches longer than twice the angle of the crossing in feet; that is to say, 9 ft. is a better length of switch to work with crossings I in $4\frac{1}{2}$ than 12 ft., and longer switches than 12 ft. can only be applied with advantage to crossings above I in 6. Facing Points should always be made the extreme length compatible with the above conditions.

The length of stock rails is a variable quantity,

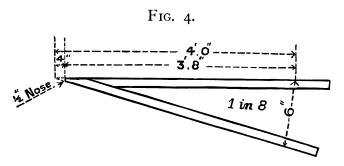
sometimes being 3 ft. or 4 ft. above the length of the point, and sometimes the standard length of the rails in use on the particular railway, but no hard and fast rule can be laid down, only due regard should be paid to allowing suitable distances at each end of the points for spacing the chairs with reference to the joints.

Crossings. The angle of a crossing is the one formed by a tangent to the curve at the point of intersection. See Fig. 3 below, in which x is the angle.

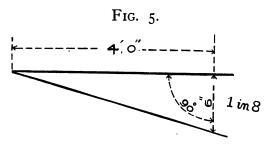


When ordering crossings to replace those in use, the simplest plan is to measure the width of the Crossing Vee across the outside of the rails at a distance of, say 4 ft. back from the nose, in which case the crossing should be specified thus—6 in. (or whatever the distance may be) at 4 ft. from actual nose of crossing, for an error is sometimes made by Platelayers when specifying crossings, due to not taking into account the thickness of the crossing

nose, thus giving the angle of a crossing which measures 6 in. at 4 ft. back from the nose, as 1 in 8, whilst, if we assume that the nose is $\frac{1}{2}$ in. thick, the actual angle, found by dividing $5\frac{1}{2}$ in. into 4 ft., is, say 1 in $8\frac{3}{4}$. This will more readily be understood by reference to Fig. 4, given below.



The above is the usual method of measuring the angle of a crossing in this country. Another plan in use on some of our Indian Railways is to measure the Vee across at right angles to one of the legs, as shown by Fig. 5.



Crossings are made right and left hand on some of our main lines, the point rail being always laid for the main way, and the splice rail for the turnout or siding; thus in fig. No. 4 the Vee shown is for a left-hand crossing to suit a curve turning off to the left hand when facing the points. For sidings they may be made all the same hand.

When measuring the angles off a drawing, care should be taken to lay down the tangent lines referred to (see Fig. 3), instead of, as is sometimes done, measuring on the curved line. It is not necessary to include fractions in the angles of crossings, except for the more obtuse ones, and those given in our tables will meet all ordinary cases, but when a fraction appears in a calculation, it is better to take the next higher rather than the lower number; for instance, suppose the angle worked out to I in $6\frac{5}{8}$, we should make the crossing I in 7, for it is easier to adapt a crossing to a situation when it is made rather too acute than the reverse. The most useful angle of crossing for sidings is 1 in 6, and for the main line, 1 in 8. With regard to the length of the various rails composing a crossing, it is impossible to lay down any hard and fast rule. For main line purposes the Vee rails vary from 8 ft. to 12 ft., and the wing rails from 12 ft. up to the full length of a standard rail, and for sidings the Vees are made from 6 ft., and the wings from 7 ft. 6 in. upwards. Check rails should always be at least 4 or 5 ft. longer than the distance between the crossing knees and the nose; but to allow sufficient latitude in fixing, and for suitably arranging the chairs and sleepers, they are generally made much

longer than the above rule indicates. For main lines a usual length is 12 ft., whilst for sidings they run from 7 to 9 ft.

Specifications for Switches and crossings for D. H. or B. H. rails standard gauge consists of the

following parts:-

SWITCHES.

- 2 Tongue Rails, 9 ft.
- 2 Stock Rails.
- 6 Cast-iron Slide Chairs.
- 2 Cast-iron Heel Chairs.
- 4 Slide Chair Bolts.
- 2 Bearing Studs.
- 4 Heel Chair Bolts.
- 2 Oak Keys.
- 1 Tie Rod.
- 1 Lever Box.
- 1 Lever Rod.

CROSSING.

- 1 Point Rail.
- 1 Splice Rail.
- 1 R.H. Wing Rail.
- 1 L.H. Wing Rail.
- 2 or more Splice Bolts.
- 4 Cast-iron Chairs.
- 6 to 8 Oak Kevs.

CHECK RAILS.

- 2 Rails.
- 6 Cast-iron Chairs.
- 6 Oak Keys.

and a full set of 12 ft. Switches and Crossings of the following parts:—

SWITCHES.

- 2 Tongue Rails, 12 ft.
- 2 Stock Rails.
- 10 Cast-iron Slide Chairs.
- 2 Cast-iron Collar Chairs, for behind heels.
- 8 Slide Chair Bolts.
- 2 Bearing Studs.
- 4 Oak Keys.
- 2 Tie Rods.
- 1 Lever Box.
- 1 Lever Rod.

Crossing.

- 1 Point Rail.
- 1 Splice Rail.
- 1 R.H. Wing Rail.
- 1 L.H. Wing Rail.
- 2 or more Splice Bolts.
- 4 Cast-iron Chairs.
- 6 to 8 Oak Keys.

CHECK RAILS.

- 2 Rails.
- 6 Cast-iron Chairs.
- 6 Oak Keys.

For flange (F.B.) rails, when these are simply fastened directly to sleepers with dog spikes, a set of 9 ft. switches and crossings consists of the following parts:—

Switches.

- 2 Tongue Rails, 9 ft.
- 2 Stock Rails.
- 8 Cast-iron Slide Chairs or Wrought-iron Sole Plates.
- 6 Slide Chair Bolts.
- 2 Bearing Studs.
- 1 Tie Rod.
- 1 Lever Box.
- 1 Lever Rod.

CROSSING.

- 1 Point Rail.
- 1 Splice Rail.
- 2 Wing Rails.
- 2 or more Splice Bolts.
- 3 Wrought-iron Sole Plates.
- 5 Cast-iron Distance Blocks.
- 6 Bolts for Distance Blocks.

CHECK RAILS.

- 2 Rails.
- 6 Cast-iron Distance Blocks.
- 6 Bolts for Distance Blocks,

and a set of 12 ft. of the following parts:-

Switches.

- 2 Tongue Rails, 12 ft.
- 2 Stock Rails.
- 10 Cast-iron Slide Chairs.
- 6 Slide Chair Bolts.
- 4 Bearing Studs.
- ² Tie Rods.
- 1 Lever Box.
- 1 Lever Rod.

CROSSING.

- 1 Point Rail.
- 1 Splice Rail.
- 2 Wing Rails.
- 2 or more Splice Bolts.
- 3 Wrought-iron Sole Plates.
- 5 Cast-iron Distance Blocks.
- 6 Bolts for Distance Blocks.

CHECK RAILS.

- 2 Rails.
- 6 Cast-iron Distance Blocks.
- 6 Bolts for Distance Blocks,

and the same specification is suitable when wroughtiron Sole Plates are used between the rails and the sleepers, but when cast-iron Chairs are used the specification should be similar to that given for D. H. and B. H. rails.

Lever Boxes in use, and every Platelayer has his own particular fancy. A perfect Lever Box should embody the following points:—

- (1) It should not take up much space.
- (2) Whilst being easy to work by the shunter, it should always bring the points home with certainty.
- (3) It should be readily changed from a "Turnover Lever," which leaves the points indifferently on one side or the other, to a "Self-acting Lever," whereby the points are always brought back to the same side.

- (4) It should possess facilities for padlocking, either to self-act always for one particular side, or to prevent it being worked at all except by authorized hands.
- (5) It should possess fewness of parts, and not be liable to get out of order.

Flangeway The factors in determining the width of flangeways between check rails and the main rail are the thickness of the wheel flange and the clearance allowed, and taking the standard gauge for example, when the flange is close up to the rail there should be at least $\frac{5}{8}$ in. clearance between the back of the flange and the check rail, which, with a flange $1\frac{1}{8}$ in. thick, allows $\frac{3}{8}$ in. clearance on the working faces, and $\frac{1}{4}$ in. clearance on the check rail side, making a total flangeway of $1\frac{3}{4}$ in.; thus when the back of the wheel flange is working close up to the check rail on the inside of the curve there is $\frac{1}{8}$ in. clearance between the working faces on the outside rail.

Platelaying. The road bed having been duly prepared and levelled by the Contractor, the material should be delivered in a manner to save unnecessary labour. The rails should be laid down in pairs end to end on one side of the road bed, and the sleepers and chairs thrown down in the numbers required for each length. The fish plates, bolts, spikes, and keys may be distributed in

heaps at convenient distances apart. Having all the material to hand, the work should proceed in the following order:-Place the sleepers on the road bed spaced approximately the required distances apart. Place the chairs upon the sleepers and lay a pair of rails loosely into them. Take a piece of chalk and with a lath properly divided set off the position of chairs on the rail. Then key the chairs to their places; adjust the sleepers to the position of the chairs. Adjust rails roughly gauge and bore all the spike holes along one side only, having sighted along it first to see that it is straight; drive a few spikes to hold the chairs in position, then set the opposite rail carefully to gauge and square across ends with the one already fixed, bore and partly drive a few spikes, making a final trial with gauge and square to see that all is in order before driving all the spikes home. the first length is laid, a second gang of men may be set to connect succeeding lengths in advance, to be adjusted and permanently spiked by the first gang in due order. The duties of a gang of platelayers, with the appropriate tools, may be divided as follows :-

- (1) Unloading and parcelling out material.

 Tools required:—Pinches and rail forks.
- (2) Fixing rails, chairs, and sleepers in their proper position. Tools required:—Tape line, T square, spirit level, road gauge, keying hammer, brace with bits, crow-

- bars, picks, jim crow, hammer adze, spades, and shovels.
- (3) Laying down and connecting succeeding length in preparation of the foregoing. Tools required:—Screw keys or wrenches, hammers, oil can, pinches, picks, clearance gauges to put in between rails at joints for giving proper space for expansion.
- (4) Ballasting or packing road level under sleepers with ashes or other suitable material. Tools required:—Picks, spades, shovels, screw rail lifters or iron shod levers, winding laths, straight edges, spirit level, crow bars, super-elevation gauge.
- (5) Boxing up and finishing, by levelling ballast to top of sleepers. Tools required:— Spades and shovels.

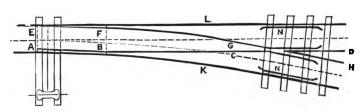
In addition to the above-mentioned there are various other tools necessary for a complete outfit, and a full list will be found on page 27.

Platelaying.
Switches and Crossings.

First lay down the sleepers for the switches and the switches, then place the switches A B E F (see Fig. 6) upon them; lay the crossing upon its sleepers, the distance from heel of switch as per tables, according to angle, seeing that each crossing chair is in the middle of its sleeper; line the crossing rail, C D, with the switch point, A B, the point being closed and not open as shown in Figure, bore and spike in this

position: fix the opposite switch, E F, to gauge tightly at point. The closing rail, F G, should next be curved tentatively (using the versed sine given in Table No. 6, for the radius corresponding to the angle as per Tables), then placed in position, adjusting it with the rail bender till it ranges properly to the eye; the crossing rails, G H, will also require setting a little to suit the curve, although it must be remembered that it is no worse for being rather flat for a few feet on each side of the crossing nose. At the switch end the aim

Fig. 6.



should be to give the curve the appearance of having sprung from a point in advance of the switches, called "spring of curve" in the Tables, otherwise there is a tendency to prolong the straight of the point rail, E F, behind the switch heels, which should be avoided. The outside rail, F G, being truly ranged and spiked down, the inside rail, K, must now be laid to gauge with it, allowing a little extra width at the crossing nose, and working rather tight to gauge for two or three feet on each side of it. We may now put in the closing rail

B C, and the opposite rail, L, to gauge with it; then fix the check rails, N N, in position, care being taken, when these are short, to see that the centre is opposite the crossing nose.

Unless the switches have been specially ordered for the right hand, the stock rail of switch, A B, will require setting in front of the point, to gauge with the opposite rail.

Special sleepers should always be provided for the crossings, the length averaging, gauge $\times 2\frac{3}{4}$, and sections from 10 in. \times 5 in. to 14 in. \times 7 in., according to the width of base of the chairs they have to carry. There should also be long sleepers of the usual sections provided for the first four slide chairs of the points, length equal to gauge, $\times 2\frac{1}{2}$, to carry the lever box, when the switches are worked by one, for when this is fixed to an isolated piece of wood, there is often a good deal of trouble caused by it shifting, with the action of the falling weight.

When fixing the Lever-box be careful to see that the weight has plenty of clearance when down, in the case of a self-acting lever, and that it falls equally on each side of the Lever Frame, in case of a turn-over lever. Coach Screws or Bolts should be used for fixing the lever frame in preference to spikes. Switches should have $3\frac{1}{2}$ in. to $3\frac{3}{4}$ in. throw at the point, and it must be seen that, at no point between the heel and where

the planed part commences, there is less than 1½ in. clearance. If the lever does not bring the points home, it is better to get it to do so by easing the bolts at the heels, and well oiling the chairs, rather than by moving the weight further along the lever. Switches are apt to work rather stiffly at first, but after the chairs have worn smooth they will be found free enough to enable them to be worked with less leverage.

Platelayer's The following is a list of what constitutes a complete set of Platelayer's Tools, for use in laying D.H. or B.H. rails on wood sleepers with cast-iron chairs:—

- 1 Ratchet Brace, with key for same, and half-adozen drills.
- 1 Wrought-iron Cramp for same.
- 1 Screw Rail Lifter or iron shod Lever.
- 1 Rail Bender, or Jim Crow, and Lever.
- 2 Keying Hammers.
- 1 Oil Feeder.
- 1 Hand Hammer.
- 2 Cold Chisels.
- 1 Rodded Chisel.
- 2 Beater Picks.
- 1 Hammer Adze.
- 1 Small Axe.
- 1 Sledge Hammer, 8 lbs.
- 1 Auger Brace and 3 bits.
- 3 Claw-ended Crowbars.

- 3 Plain ended crowbars.
- 3 Pinch Bars.
- 2 Disc Signals.
- 2 Flag Signals.
- 2 Screw Keys.
- 1 Shifting Spanner.
- 6 Steel Shovels.
- 3 Steel Spades.
- 2 Rail Forks.
- I Graduated Spirit Level, for fixing superelevation of outer rail on curves.
- 1 Road Gauge.
- 1 Footway do.
- 1 Straight Edge.
- 1 T-Square.
- 2 Winding Strips or Sighting Boards, with clips to fasten them to the rails.
- 1 10-inch Spirit Level.
- 1 Flat Bastard File.
- 1 Three-square do.
- 1 Metallic Wired Measuring Tape.
- I Large Box, to contain the above tools, with padlocked lid.
- 1 Trolley.

Memoranda. The best Permanent Way consists of bull-head steel rails, keyed into castiron chairs, and spiked to creosoted sleepers. When flange rails are used, one of the best systems is a wrought-iron soleplate, rolled with a groove to take

the rail flange, having a hole at each side of groove to take a coach screw with deep-cut buttress threads, and a mushroom head, which impinges partly on the rail flange and partly upon the soleplate. These are screwed into the sleepers with a key applied to a square boss projecting from the head.

An excellent permanent way can be made with flange rails placed upon plain wrought-iron soleplates punched with four holes, through which four dog-eared spikes are driven into the sleeper, two on each side of the rail.

Flange rails fastened direct to sleepers with two or three dog spikes per yard make a good enough road for wagon sidings and temporary work.

The transverse strength of flange rails weight for weight is greater than that of Bull Head or Double Head Sections. The radii at the top corners of rail head should always be considerably less than the radius of fillet in the wheel flange. A large top radius of the head for the sake of adhesive surface is important. A top radius of 14 inches, with corner radii of $\frac{5}{16}$ in., gives good results.

The less the surface of a rail is interfered with the better, and notching should be avoided as much as possible.

Chairs should have either two spikes and two trenails, or three spikes, on curves. Two spikes, or two spikes and one trenail, are generally sufficient for straight road.

There is little or no advantage in jagging or

twisting spikes. One of the best forms consists of a round parallel shank swelled in the neck to fairly fill the tapered chair hole, and bevilled slightly at the point to facilitate driving.

Sleepers, except for temporary work, should be creosoted with 9 or 10 lbs. of creosote per cubic foot. The chairs should be laid on the sawn or heart side and bedded level. Sleepers at the joints should be laid only $\frac{3}{4}$ to $\frac{4}{5}$ ths of the distance apart of the intermediate ones.

Old spike holes in sleepers should be filled by oak trenails tarred and driven very tight.

Spike holes should be about one-fourth less than diameter of spikes, and bored right through the sleeper.

Diamond Crossings should not be put in of a more acute angle than 1 in 8 where locomotives are used, and it is well where practicable to keep them down to 1 in 6.

In places where there is a tendency for the couplings to catch in the vees of the crossings, these should be fitted with blocks of wood inside of the rails; and where horses are used for hauling, the open ends of check rails and crossings should be protected by pieces of wood nailed to the sleepers.

Standard Dimensions, 4 ft. $8\frac{1}{2}$ in. Gauge.

Flangeway Clearance, $1\frac{3}{4}$ in. to $1\frac{7}{8}$ in., according to thickness of wheel flanges.

Clearance between wheel flanges and rails, $\frac{3}{8}$ in.

Travel of points at end, $3\frac{1}{2}$ in. to $3\frac{3}{4}$ in.

Tilt, or inclination of rail inwards, and cone of wheels, 1 in 20.

Vertical flangeway clearance from top of rails, $1\frac{1}{2}$ in. to $1\frac{3}{4}$ in.

Footway, or distance between lines of way inside of rail heads—

Sidings (minimum) 5 ft.

Main way (Board of Trade minimum) 6 ft.

Vertical height above rail level for bridges, &c., minimum, 14 ft. 6 in.

Sleepers, 9 ft. \times 10 in. \times 5 in.

Crossing sleepers, 12 ft. to 14 ft. \times 12 in. \times 6 in. to 14 in. \times 7 in.

Sleepers (intermediate), centre and centre, 2 ft. 9 in. to 3 ft.

Sleepers (joint), centre and centre, 2 ft. 4 in. to 2 ft. 6 in.

The minimum distance between the two lines of way to allow trucks to clear, 3 ft. 9 in.

Minimum depth of ballast below sleepers, 8 in.

Length of spikes, 6 in.

Clearance between rail ends to allow for expansion when laid in cold weather, $\frac{3}{16}$ in.

Minimum width of wheel tread that will safely run over a crossing, 4 in.

On wagons for sidings, minimum width of tyres, 4½ in.
and on engines and wagons for main line, 5 ins.

Maximum width of wheel tread, 6 in.

Wheel flange should not exceed in depth $1\frac{1}{4}$ in.

Board of Trade Regulations referring to Main Lines.

Minimum distance of standing work from outer edge of rails at level of carriage steps, 3 ft. 6 in.

Switch handles not to be worked between lines of railway.

Facing Points to be avoided, but where unavoidable to be provided with locking bars and signals.

Catch points to be provided on sidings falling towards the main line.

Joints of rails to be fished.

Chairs to be secured by iron spikes.

TABLES AND DIAGRAMS,

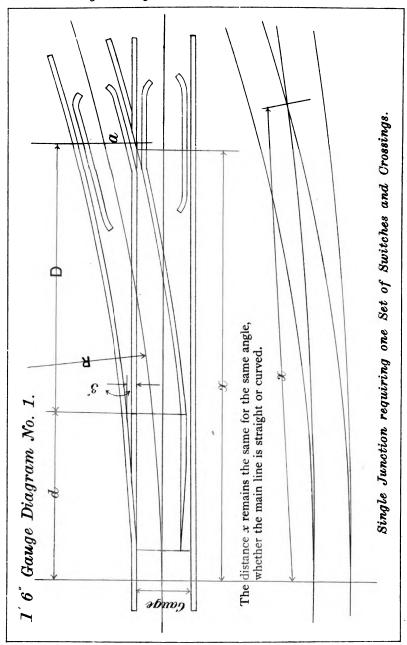
CONTAINING

TABLES FOR THE FOLLOWING GAUGES:-

1 ft. 6 in., 2 ft. 0 in., 2 ft. 6 in., 3 ft. 0 in., 3 ft. $3\frac{1}{8}$ in., 3 ft. 6 in., 4 ft. $8\frac{1}{8}$ in., 5 ft. 3 in., and 5 ft. 6 in.,

REFERRING TO

Diagrams for Single Junctions, Double Junctions,
Three-Throws, Single Through Roads,
Double Through Roads, Diamonds with Single Slips,
and Diamonds with Double Slips.

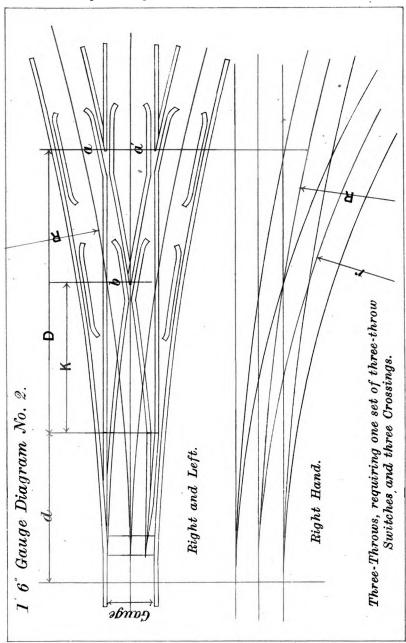


1 ft. 6 in. Gauge. Table No. 1.

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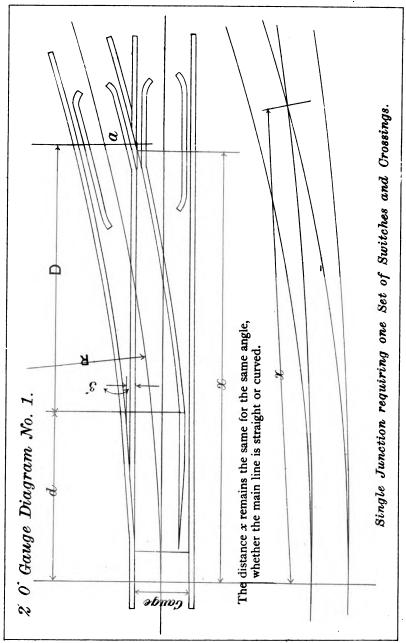
SINGLE JUNCTIONS.

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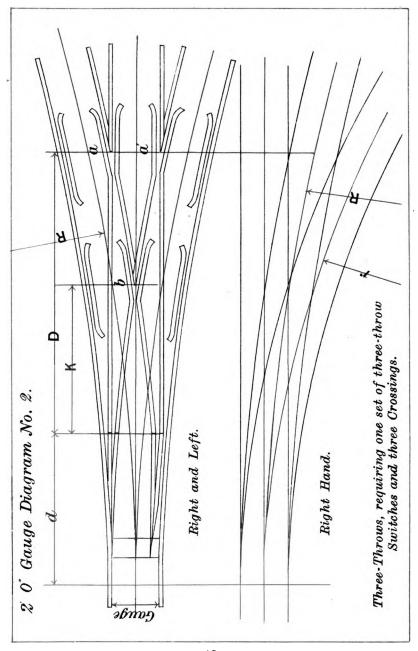
THREE THROWS. 1 ft. 6 in. Gauge. Table No. 2.

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2 ft. 0 in, Gauge. Table No. 1.

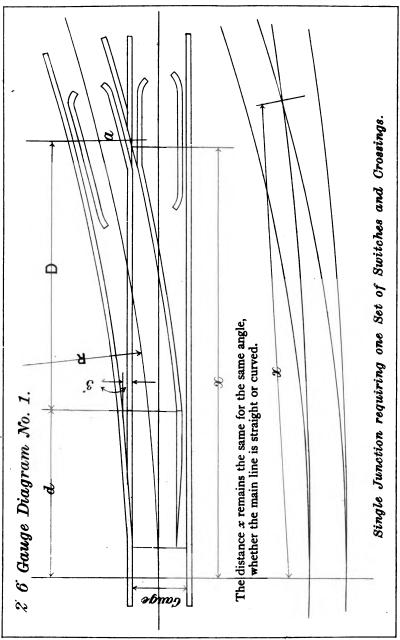
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CA	D Heel of Switches to Nose of Crossing.	Fr. Ins. 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	d Spring of Curve to Meel of Switches.	F. II. 2 2 2 2 3 3 3 2 2 5 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2
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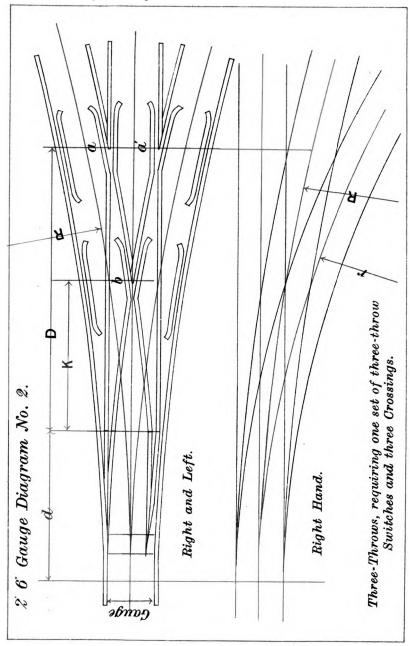
2 6 Gauge Diagram No. 1.



2 ft. 6 in. Gauge. Table No. 1.

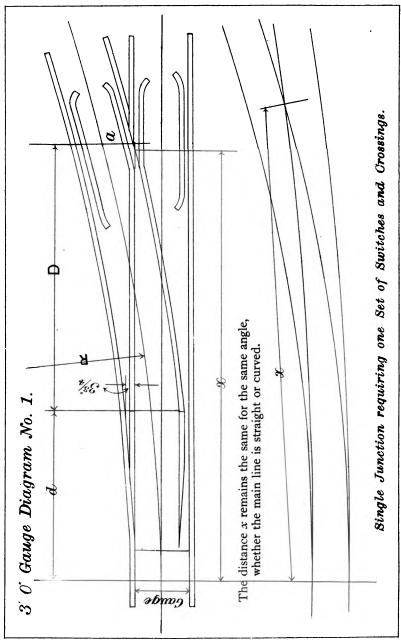
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SINGLE JUNCTIONS. 6 in. Gauge. Table No. **2**



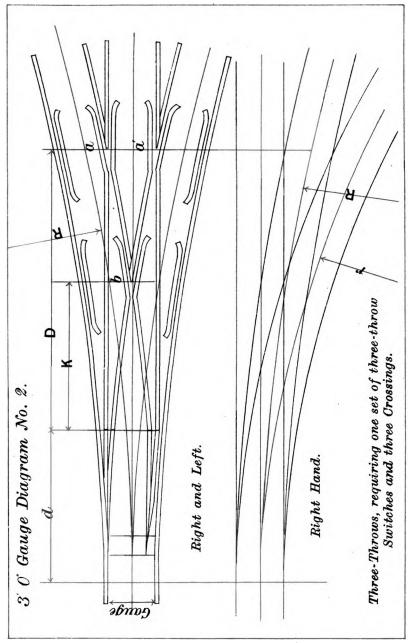
THREE THROWS. 2 ft. 6 in. Gauge. Table No. 2.

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Radius of Inside Curve.						326	250	277	303	331	360	391	423	490	563	640	723	810	
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Radius of Curve.	Ft. In					38													245
Curve.	표	15	70	25	31		45	53		70	8	8	102	113	125	152	180	212	245
	표	9 15	0 50	9 25	9 31	38	6 45	6 53	0	9	08	9	0 102	0 113	0 125	0 152	0 180	0 212	245
Radius of Inside	Ft. Ins. Ft.	7 9 15	10 0 20	12 9 25	15 9 31	19 0 38	22 6 45	26 6 53	31 0 61	35 6 70	40 0 80	45 6 90	51 0 102	57 0 113	63 0 125	76 0 152	90 0 180	106 0 212	0 245
Curve.	Ins. Ft. Ins. Ft.	74 7 9 15	o 2 10 0 20	64 12 9 25	o4 15 9 31	0 38	0 22 6 45	6 26 6 53	114 31 0 61	54 35 6 70	11½ 40 o 80	5 45 6 90	114 51 0 102	54 57 0 113	111 63 0 125	11 76 0 152	11 90 0 180	11 106 0 212	101 123 0 245
to Mose of Crossings Heel of Switches to Mose of Crossing Market of Inside Curve.	Ft. Ins. Ft. Ins. Ft.	3 74 7 9 15	4 04 10 0 20	4 64 12 9 25	5 0\frac{1}{8} 15 9 31	5 6½ 19 o 38	6 0 22 6 45	6 6 26 6 53	6 114 31 0 61	7 54 35 6 70	7 114 40 0 80	8 5½ 45 6 90	8 11 5 51 0 102	9 54 57 0 113	9 113 63 0 125	10 11 76 0 152	081 0 06 11 11	12 11 106 0 212	13 101 123 0 245
Heel of Switches to Mose of Crossing. Description of Inside Curve.	Ins. Ft. Ins. Ft. Ins. Ft.	04 3 74 7 9 15	II 4 04 IO 0 20	9 4 6 12 9 25	7 5 04 15 9 31	$6\frac{1}{8}$ 19 o 38	43 6 0 22 6 45	24 6 6 26 6 53	14 6 114 31 0 61	113 7 54 35 6 70	9 2 7 11½ 40 0 80	8 8 5 45 6 90	61 8 II 5 51 0 102	54 9 54 57 0 113	$3\frac{1}{3}$ 9 11 $\frac{1}{3}$ 63 0 125	0 10 11 76 0 152	84 11 11 90 0 180	5 12 11 106 0 212	2 13 104 123 0 245
Heel of Switches as a self of Switches as a self self self self switches to Nose of Crossing by Switches by Switches by Nose of Crossing by Switches by Nose of Inside self self self self self self self sel	s. Ft. Ins. Ft. Ins. Ft. Ins. Ft.	6 03 3 74 7 9 15	\$ 6 II 4 04 IO 0 20	1 9 4 6 12 9 25	1 8 7 5 0 1 15 9 31	$6 5 6\frac{1}{2} 19 0 38$	1 IO 41 6 0 22 6 45	1 II 2 6 6 26 6 53	1 12 14 6 114 31 0 61	12 113 7 54 35 6 70	13 94 7 II 40 0 80	1 14 8 8 5½ 45 6 90 B	15 64 8 114 51 0 102	16 5\frac{2}{4} 9 5\frac{1}{2} 57 0 113	$\frac{1}{8}$ 17 $3\frac{1}{2}$ 9 $11\frac{1}{2}$ 63 0 125	19 0 10 11 76 0 152	1 20 81 II II 90 0 I80	22 5\frac{1}{3} 12 11 106 0 212	8 24 2 13 10s 123 0 245
Heel of Switches Heel of Switches to Mose of Crossings Rel of Switches to Nose of Crossing to Nose of Crossing Redires of Inside	Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft.	9 6 04 3 74 7 9 15	1\frac{2}{4} 6 II 4 0\frac{2}{4} IO 0 20	$3 6\frac{1}{8} 7 9\frac{1}{8} 4 6\frac{2}{8} 12 9 25$	$3 \times 11\frac{1}{4} \times 8 \times 7 \times 5 \times \frac{1}{9} \times 15 \times 9 \times 31$	$4 + 4 + 9 + 6 + 5 + 6\frac{1}{2} + 19 + 0 + 38$	4 8\frac{2}{3} \text{ IO 4\frac{1}{2} \text{ 6 O 22 6 45}	5 13 11 23 6 6 26 6 53	5 64 12 14 6 114 31 0 61	$5 \text{ II} \left[12 \text{ II} \frac{1}{8} \right] 7 5\frac{3}{4} 35 6 70$	6 3 ³ / ₄ 13 9 ² / ₄ 7 11 ¹ / ₂ 40 0 80	6 $8\frac{1}{8}$ 14 8 8 $5\frac{1}{2}$ 45 6 90	7 1 15 64 8 114 51 0 102	7 6 16 54 9 54 57 0 113	$7 \log^{\frac{1}{2}} 17 3^{\frac{1}{2}} 9 11^{\frac{1}{2}} 63 0 125$	8 8 19 0 10 11 76 0 152	9 53 20 83 11 11 90 0 180	10 3 22 5\frac{1}{8} 12 11 106 0 212	81 08 24 2 13 108 123 0 245
Spring of Curve to the of Switches. Heel of Switches as a line of Crossings Heel of Switches as a line Meel of Switches of Crossing Kadius of Crossing Padius of Inside	Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft.	9 6 04 3 74 7 9 15	9 3 14 6 II 4 04 IO 0 20	$3 6\frac{1}{8} 7 9\frac{1}{8} 4 6\frac{2}{8} 12 9 25$	$3 \times 11\frac{1}{4} \times 8 \times 7 \times 5 \times \frac{1}{9} \times 15 \times 9 \times 31$	$93 + 4 + 9 6 + 5 6\frac{1}{8} + 19 0 + 38$	10 4 8\frac{1}{2} 10 4\frac{1}{2} 6 0 22 6 45	28 5 13 11 24 6 6 26 6 53	46 5 64 12 14 6 114 31 0 61	64 5 11 12 113 7 54 35 6 70	$82 6 3\frac{3}{4} 13 9\frac{2}{4} 7 11\frac{1}{3} 40 0 80$	6 $8\frac{1}{8}$ 14 8 8 $5\frac{1}{2}$ 45 6 90	17 7 1 15 64 8 114 51 0 102	34 7 6 16 53 9 53 57 0 113	$52 \mid 7 \text{ lo}\frac{1}{8} \mid 17 3\frac{1}{8} \mid 9 \text{ li}\frac{1}{8} \mid 63 \text{ o} \mid 125$	88 8 8 19 0 10 11 76 0 152	23 9 5\frac{1}{2} 20 8\frac{1}{2} 11 11 90 0 180	58 10 3 22 51 12 11 106 0 212	94 11 04 24 2 13 104 123 0 245
Spring of Curve to the of Switches. Heel of Switches as a line of Crossings Heel of Switches as a line Meel of Switches of Crossing Kadius of Crossing Padius of Inside	Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft.	in 1.21 2 9 6 04 3 74 7 9 15	in 1.39 3 14 6 11 4 04 10 0 20	in 1.57 3 $6\frac{1}{8}$ 7 $9\frac{1}{8}$ 4 $6\frac{3}{4}$ 12 9 25	in 1.75 3 114 8 7 5 04 15 9 31	$93 + 4 + 9 6 + 5 6\frac{1}{8} + 19 0 + 38$	in 2'10 4 8\frac{2}{4} \text{ IO 4\frac{2}{3} \text{ 6 O 22 6 45}	in 2'28 5 13 II 23 6 6 26 6 53	in 2'46, 5 64 12 14 6 114 31 0 61	in 2.64 5 11 12 11\frac{1}{3} 7 5\frac{3}{4} 35 6 70	in 2.82 6 3\frac{3}{4} 13 9\frac{2}{4} 7 11\frac{1}{2} 40 0 80	in 3.00 6 $8\frac{1}{8}$ 14 8 8 $5\frac{1}{8}$ 45 6 90	in 3.17 7 1 15 64 8 114 51 0 102	in 3:34 7 6 16 54 9 54 57 0 113	in 3.52 7 $10^{\frac{1}{2}}$ 17 $3^{\frac{1}{2}}$ 9 $11^{\frac{1}{2}}$ 63 0 125	in 3.88 8 8 19 0 10 11 76 0 152	in 4.23 9 5\frac{1}{2} 20 8\frac{1}{2} II II 90 0 180	in 4.58 10 3 22 5\frac{1}{3} 12 11 106 0 212	in 4'94 BI OB 24 2 I3 IOB 123 O 245
Spring of Curve Spring of Curve Heel of Switches to Nose of Crossings Relof Switches to Nose of Crossing K	Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft.	1 in 1.21 2 9 6 04 3 74 7 9 15	1 in 1.39 3 14 6 11 4 04 10 0 20	$ 1 \text{ in } 1.57 3 6\frac{1}{8} 7 9\frac{1}{8} 4 6\frac{3}{8} 12 9 25$	1 in 1.75 3 112 8 7 5 03 15 9 31	in 1.93 4 4 9 6 5 $6\frac{1}{8}$ 19 0 38	1 in 2 10 4 84 10 44 6 0 22 6 45	1 in 2.28 5 13 11 23 6 6 26 6 53	1 in 2'46, 5 64 12 14 6 114 31 0 61	$1 \sin 2.64 5 \text{ II} 12 \text{ II} 7 5\frac{3}{4} 35 6 70$	$1 \text{ in } 2.82 6 3\frac{3}{4} 13 9\frac{2}{4} 7 11\frac{3}{2} 40 0 80$	1 in 3 oo 6 8 1 14 8 8 5 1 45 6 90	1 in 3.17 7 1 15 64 8 114 51 0 102	1 in 3.34 7 6 16 54 9 54 57 0 113	$ \text{r in 3.52} 7 \text{ lo}_{\frac{1}{8}} \text{ li } 3\frac{1}{2} 9 \text{ li}_{\frac{1}{8}} 63 \text{ o} \text{ li25}$	1 in 3.88 8 8 19 0 10 11 76 0 152	$1 \sin 4.23 + 9 + 5\frac{1}{8} = 20 + 8\frac{1}{8} = 11 = 11 + 90 = 180$	1 in 4.58 10 3 22 5\frac{1}{2} 12 11 106 0 212	1 in 4'94 11 0\frac{1}{3} 24 2 13 10\frac{1}{3} 123 0 245



3 ft. 0 in. Gauge. Table No. 1.

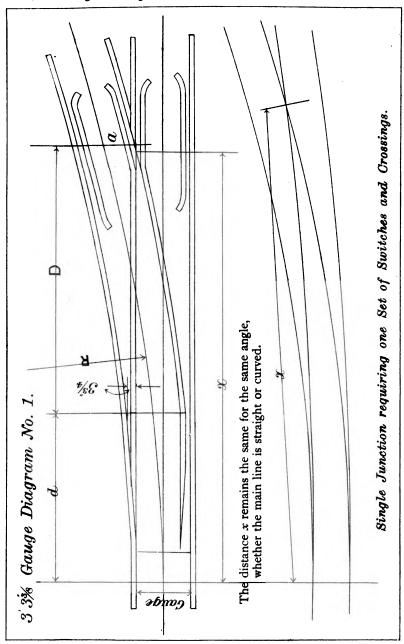
		Radius of Curva.	i 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	٠	<u> </u>	13.5 13.8 13.8 13.8 13.8 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10
		intersection of Gauge Lines.	ii 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
		Spring of Curve to	73 4 4 5 4 4 5 4 4 5 4 4 5 4 4 5 4 4 5 4 4 5 4 4 5 4 4 5 4 4 5 4 4 6 6 6 6
		D Heel of Switches to Mose of Crossing.	Ins. 110 94 94 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
		O TOP	F. F
		to Heel of Switches.	and 20 20 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
	1.	Spring of Curve	7 4 7 7 7 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8
		In degrees.	M. M
Ž	Table No.	Angle of Crossing.	9 0 0 0 N N N 4 4 4 4 4 4 4 4 4 4 4 4 4 4
P	Tat	stian al	48 88 84 88 84 88 84 88 88 88 88 88 88 8
S S		Angle of Crossing.	B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.
3	g e.	VORTING OF CHIPS.	00000000000000000000000000000000000000
SINGLE JUNCTION	Gauge.	Radius of Curve.	Ft. 136 934 934 934 934 934 934 934 934 934 934
Ž	in.	Spring of Curve to intersection of Gauge Lines.	<u>ដ</u>
•	ft. 0	Spring S	10 11 11 11 12 12 13 14 15 15 15 15 15 15 15 15 15 15 15 15 15
	က	to Nose of Crossing.	E 4 4 7 5 5 5 6 7 7 7 9 9 6 7 9 9 9 9 9 9 9 9 9 9 9 9
		D Heel of Switches	7
		Hoel of Switches.	140 4844 0 648 18 14 16 16 18 18 18 18 18 18 18 18 18 18 18 18 18
		d Spring of Curve	F 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
		In degrees.	MF 2 4 48 88 88 4 4 8 8 8 9 8 8 9 8 8 9 8 8 9 8 8 9 8 9
		Angle of Crossing.	0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		estion al	# n n n n n n n n n n n n n n n n n n n
		Angle of Crossing.	



THREE THROWS. 3 ft. O in. Gauge. Table No. 2.

īs. 0 0 0 0 0 0 0 0 0 H Radius of Curve. Ft. 338 338 384 434 486 660 660 726 726 738 117 Radius of Inside K Heel of Switches to Mose of Crossing. Ins. 93 2 ~ 8 0 E D Heel of Switches to Mose of Crossings. Ft. 33 34 34 35 41 41 41 0 1 0 0 0 Heel of Switches. Spring of Curve Angle of Crossing. 1000 000 0 1000 000 0 (이 I 222222222222222222 Angle of Crossings. # m o m o o o o o o o o o o o o o o Radius of Curve. an lo suribasi るななはなななならいっとのに K Heel of Switch to Mose of Crossi **温みまるがで 4444500047880**0 Heel of Switch 140 + 8xxxx 0 6xx 18 Heel of Switch Spring of Curve 肌 ろう 4 4 5 50 6 7 7 8 8 8 8 8 9 8 1 1 1 1 1 1 Angle of Cros ה מממטטטטט 4444505000 p Angle of Cro. -----

3'3% Gauge Diagram No. 1.

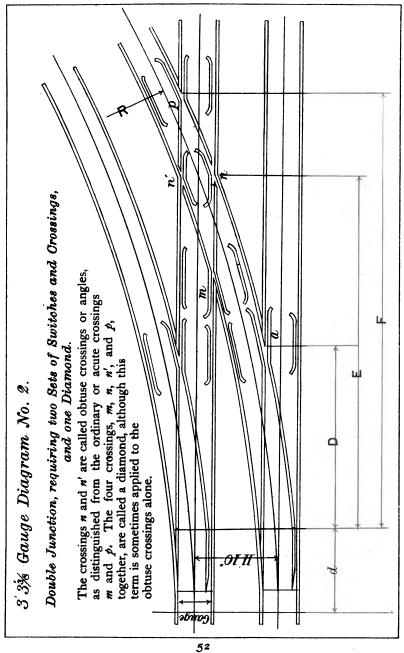


3 ft. 3% in. Gauge. Table No. 1.

		_																		
	Radius of Curve.	ä	0	0	0	0	0	0	0		0		0			0			0	
	<u>я</u>	F	369	420	474	532	592	929	724	794	898	945	1025	1109	1286	1476	1680	1896	2126	
	intersection of Gauge Lines.	ŝ	2	9	6	0	4	~	1 1	81	Ŋ	6	0	3	10	Ŋ	11	9	H	
	Spring of Curve to	Ft. 1			55		62	65	89	72	75	78	82	85	16	86	104	111	118	
	D Heel of Switches to Nose of Crossing.	Ins.														10		11	7	
	a	ł						45	84	20	52	55	57	59	64	68	73	11	82	
	Heel of Switches.	Ins.	다	13	H	1 2	a	(1	(1	64	0	(4	61	0	3	e	"	~	3	
1.	d Spring of Curve	Ę	15	16	17	81	61	20	21	7	23	24	25	5 0	28	30	32	34	36	
No.	Angle of Crossing. and degrees.										58	9	36	24		20				
Table		ă	_	_	9	<u> </u>	<u> </u>	2	2	S	4	4	4	4	4	~	<u>س</u>	· "		
Tal	Angle of Crossing. 8 In units.										n III		n 123		n 14	in 15	91 u	11 u	81 u	
	adirect) to efect		-	ı		-	-	–		ı	-		Ι.	Ι		Ή.		H	Ξ.	
Gauge.	Radius of Curve.										9					٥				
		F	8	97	33	41	2	59	<u></u>	8	92	105	119	133	148	164	199	237	278	322
3% in.	Spring of Curve to intersection of Gauge Lines.	Ins.	5 2	Ha Ha	6	4	0 18	\$	4	I I	74	က	10	9	71	10	H	4	∞	11
13	x .	땶	11	13	14	16	2 1	19	2 I	22	24	3 6	27	29	31	32	36	39	42	45
3	Heel of Switches to Mose of Crossing.	Ins.	0	2	4	S 4	72	- t	11	0 0	2	44	9	7	93	1 I ½	n	€ 9	01	-jes
	a	표	∞	6	01	11	12	13	14	16	17	18	19	20	21	7	25	27	50	32
	Spring of Curve to Heel of Switches.	Ins.	9	- 	1 0	6	19	0	79	- 1 70	- 10 10 10 10 10 10 10 10 10 10 10 10 10 1	~ % O	-is	-	7	-	-	=	-	
	p P	Ft	3	4	4	v	'n	છ	9	_	7	∞	∞	0	0	°	II	13	13	14
	g. In degrees,	Min.	52	4	4	38	36				12	14	92	9		56				2
	Angle of Crossing.	Deg	31	200	25	22	20	18	17	9_	15	14	13	12	12	11	2	6	∞ 	∞
	a. In units.															5				
	Angle of Crossing.				ı			1 10				Ξ.	Ξ.	Ξ.		<u> </u>		묘.	ı.	;;

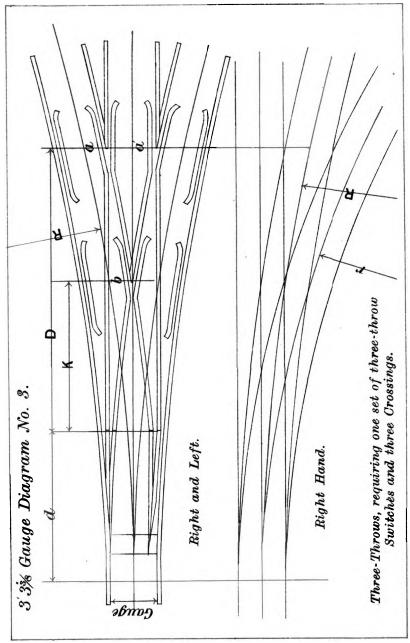
SINGLE JUNCTIONS.

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_		3 ft. 3% in. Gauge. Table No. 2.
	Radius of Curve.	Fi.Ins. 330 o 330
	Heel of Switches to Nose of Crossing.	Fi. Ins. 89 10 10 10 10 10 10 10 10 10 10 10 10 10
	Heel of Switches to Knees of Crossing.	77. In. 17. In. 18. In
	Heel of Switches to Mose of Crossing.	80
!	Spring of Curve to Heel of Switches.	Ft. In 15 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	Angle of Crossing.	H H H H H H H H H H H H H H H H H H H
6.	Angle of Crossings.	3.3.77 3.3.77 3.3.77 3.3.77 3.3.77 3.3.71
e No.	Angle of Crossing.	4 4 6 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Table	<u> </u>	7.7% 1 in 1
	Radius of Curve. Angle of Crossing.	
g e.	d H	Ft.I 202 33 33 33 32 32 32 32 32 32 32 33 32
Gauge.	Heel of Switches to Mose of Crossing.	7f. Ins. 27
3 _{\$} in.	E Heel of Switches to Knees of Crossing n	下: 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
3 ft. 3	D Heel of Switches to Nose of Crossing.	Fi. 1 Fi
•	Spring of Curve to to Heel of Switches,	T. w44 2200 0 5 5 8 9 9 9 9 1 1 2 5 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	Angle of Crossing.	1 in 68 1 in 952 1 in 195 1 in 195 1 in 195 1 in 195 1 in 193 1 in 2.17 1 in 2.25 1 in 2.76 1 in 2.76 1 in 2.76 1 in 2.76 1 in 2.76 1 in 2.76 1 in 3.30
	Angle of Crossing.	1 in 2.3 1 in 3.3 1 in 3.3 1 in 3.3
	Angle of Crossing.	10.00
	Angle of Crossing.	1 in 1 '99 i
	Angle of Crossing.	######################################

DOUBLE JUNCTIONS.

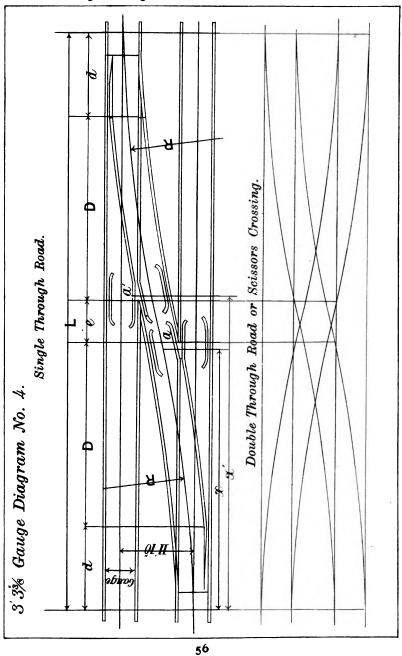


THREE THROWS. 3 ft. 3s in. Gauge. Table No. 3.

														_						
		Ins.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	Radius of Curve.	Ft.	369	420	474	532	592	656	724	794	898	945	1025	1109	1286	1476	1680	1896	2126	
١	Curve.	lns.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	Padius of Inside										434	473	513	555	643	738	840	948	1063	
	to Nose of Crossing.	Ins.	11	3	7	11	3	7	10	(1	9	0	8	9	0	6	S	H	6	
	Kel of Switches	F	19	21	7	23	25	5 0	27	29	30	31	33	34	37	39	42	45	47	
	to Nose of Crossings.	Ins.	'n	8	0	3	~	IO	8	Ŋ	6	-	4	∞;	63	01	4	11	7	
	Heel of Switches			36	39	41	43	45	84	20	52	55	57	59	9	89	73	11	82	
	Heel of Switches.	Ins	T S	H 8	I B	I 2	8	8	8	8	8	8	8	8	"	3	3	3	"	
,	Spring of Curve	Ft	15	91	11	18	19	9	21	7	23	24	25	56	8	30	32	34	36	
5	~~~~~		62.5	29.5	9.6	5.36	5.71	90.	1.42	1.17	8.12	3.48	3.84	61.6	68.6	9,0	1.31	2.05		
	Angle of Crossing.		ij.	.달	ם.	ם.	.드	ij.	ם.	ם.	.5		.5	.9	.5	12.	in	<u>:</u>	=	
					$8\frac{1}{2}$ I	6	931	0	$10\frac{1}{9}$	11 1	IIBI	7	2 1 I	3	14 1	2	9	17 1		
	Angle of Crossings.		ı in	ı in							.=	ııı	ı in ı			ı in ı	ı in ı	ı in	_	
p		s	0	3	9	•	0	0	9	9	9	0	0	0	0	0	0	0	0	0
	Radius of Curve.	1									92									
		ns.	0	n	6	9	6	9	0	9	9	9	9	9	0	0	9	0	0	0
'	Radius of Inside Curve.	Ft. I	10	13	91	20	24	29	35	9	46	25	59	99	74	83	66	118	139	191
)	d descritor	Ins.	86	5	14	6	'n	0 하	 	4	4		4	I I	∞	312	∞	[13]	ري داه	73
	K Heel of Switches to Mose of Crossing.	1 .									01									
	to Mose of Crossings	Ins.	٥ اه	24	4	5. 4.	73	8 ₁		0	7 7 8	4	9	72	912	- FI	~	63	2	T S
	D Heel of Switches to Nose of Crossings										11									
	to Switches.	Ins.	9	04	6,1	45	<u>6</u> ³	031	61	0 2 2	7 8	-\s	- 10 10 10 10 10 10 10 10 10 10 10 10 10	_	7	_	-	н	-	-
	Spring of Curve	Ft.	ę	4	4	S	ĸ	9	9	7	7	∞	∞	6	6	ួ	11	12	13	14
	_		.21	.39	.27	.75	.63	01.	.30	.40	5.64	82	8	11	.34	.52	88.	.23	.28	1.64
	Angle of Crossing.		r in 1			Ξ.	.5	멸.	.2	Ξ.	ı in 2	=		ם.	.9	Ξ.	.8	.드	.=	. E
	Angle of Crossings, 8 8!	_	2 4	~	24			_			34									
											ı									
																				_

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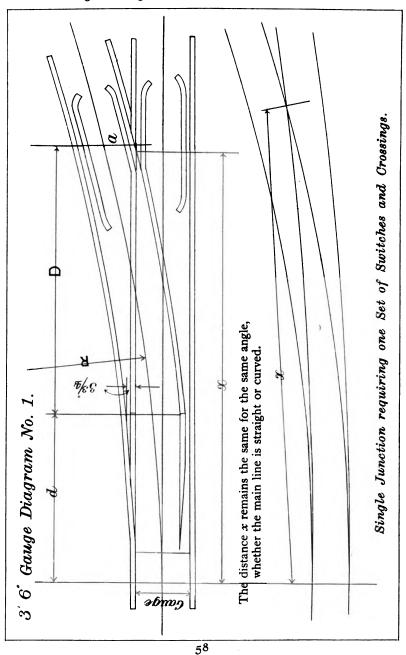
3'3% Gauge Diagram No. 4.



3 ft. 3¾ in. Gauge. Table No. 4.

### THROUGH ROAD. Applied of Countries A				
### Contract Contracts			Radius of Curve.	
THROUGH ROAD. 3. Th. 33e in. Gauge. Angle a s s s s s s s s s s s s s s s s s s			Spring of Curve to Spring of Curve.	Ins.
THROUGH ROAD. 3. 11. Gain Gauge Angle of Carree Springs of Curve to Springs of Springs of Springs of Curve to Springs of Springs of Springs of Curve to Springs of			Spring of Curve to interesting	11.5
THROUGH ROAD. THROUGH ROAD. 3. ft. 35; in 12, 37; in		. i	intersection of Gauge Lines at Crossing &	11 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
THROUGH ROAD. Aft. 39: in. Gauge. Ft. Ins. Ft.	•		Crossings.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
THROUGH ROAD. Angle of Coossings	,		to Mose of Crossings.	7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
Arthur Course at the control of the	ġ	ble No	Spring of Curve to	NXXXX
THROUGH. Angle of Crossings. Angle of Crossings.		Ta	8.81	788 6 6 6 7 7 7 1 1 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2
Angle of Crossings. T. 1. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.	POOF	lauge.	Radius of Curve.	
Angle of Crossings. Angle of Crossings. Angle of Crossings. Angle of Crossings. T. Ins. 74 A 5 6 6 6 7 11 Angle of Crossings. T. Ins. 74 A 6 6 7 12 A 7 6 7 7 7 7 7 10 B 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	THR	ij	Spring of Curve to Spring of Curve.	10 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
Angle of Crossings. T. I. I. Spring of Curve to Crossing Spring Spri		돢	intersection of Gauge	100 1 1 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Angle of Crossings. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2			intersection of Gauge Lines at Crossing a	11 8 8 4 9 4 8 4 1 1 1 8 8 4 9 4 9 1 1 1 8 8 4 8 4 1 1 1 1 1 1 1 1 1 1 1 1
in ii i			Crossings, R. B.	######################################
i. i			to Mose of Crossings.	1004481010140101 0001 1004481
コード・コード・コード・コード・コード・コード・コード・コード・コード・コード・			Spring of Curve to Meel of Switches.	ZXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
			a a	# XXX XXX XXX X X X X X X X X X X X X X

3' 6' Gauge Diagram No. 1.

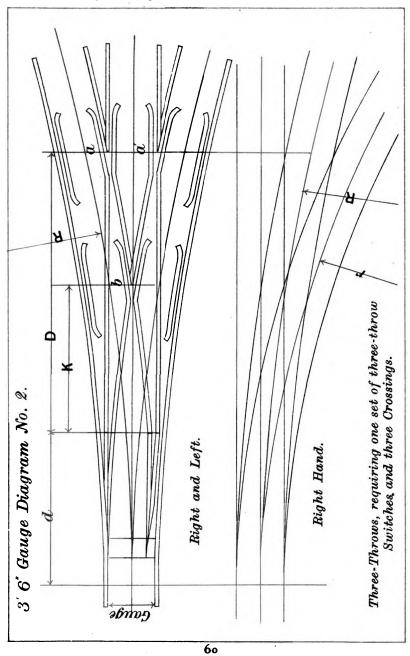


3 ft. 6 in. Gauge. Table No. 1.

										•	••••		ia.	'8'	٥.	•	a.	,,,		· · ·
	Radius of Curve.	Ft. Ins.					632 0						1094 0	0 8811				2023 0	2268 0	
	Spring of Curve to intersection of Gauge Linea.						9 99													
	D Heel of Switches to Nose of Crossing.	Ft. Ins.			42 2		47 2	49 7		54 7	57 I	59 6		64 6						
1.	d Curve Spring of Curve to Heel of Switches.						6 61						0 92	27 I				35 5		
Table No.	Angle of Crossing. In degrees.	Deg. Min.	7 38	7 10	6 44	6 22	7	5 44	5 26	5 12	4 58	4 46	4 36	4 24				3 22		
Tal	Angle of Crossing.						ı in 94											r in 17		
Gauge.	Redius of Curve.						53 0						127 0					252 0	0 962	343 0
ft. 6 in.	Spring of Curve to intersection of Gauge Lines.	Ft. Ins.																	45 6	
3	D Heel of Switches to Mose of Crossing.	ι.		•	11 24			•				• •							32 3	
	d Spring of Curve to Heel of Switches.																		13 64	
	Angle of Crossing.	Deg. Min.	31 52	28 4	25 4	22 38	20 36	18 54	17 26	91 91	15 12	14 14	13 26	12 40	12 2	11 26	10 24	9 32	8 4 8	% 01 8
	Angle of Crossing.																		in 64	

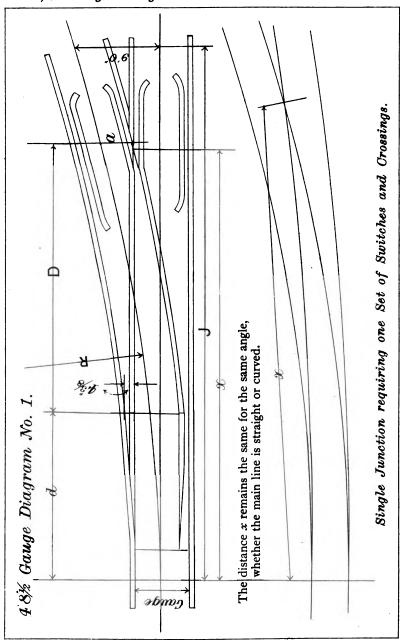
SINGLE JUNCTIONS.

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THREE THROWS. 3 ft. 6 in. Gauge. Table No. 2.

								_											
	Ins.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Radius of Curve.						632													
	-	<u>_</u>	4	-	-	<u>•</u>	_	_											
Curve.						0				0		0				0		0	
Radius of Inside	표	191	324	253	2 8	316	350	386	424	463	504	547	592	989	788	896	012	134	
a	si B	6	70	∞	н	7	0	2		4	<u> </u>	3	∞	_	'n	4	<u>-</u>	~	
Heel of Switches to Mose of Crossing.	l .					27													
, , , , , , , , , , , , , , , , , , ,									_	_				_	_	_	_	_	
to Mose of Crossings.						81			7			0							
Heel of Switches	F	37	39	42	44	47	49	52	54	57	59	62	64	69	74	79	84	8	
	·š	7	00	<u> </u>	6	6	<u> </u>	9	-	-	0	_	_	~		+		9	
Spring of Curve to Heel of Switches.																			
p p	Ĕ					19						92							_
		62.	9.9	8	.30	14.9	90.	.42	11.	.12	. 4 8	•84	61.	8	9,0	.31	.03	2.12	
Angle of Crossing.																			
		H	-	=	H	H	H	H	H	-	-	H	-	=	=	-=	Ξ	=	
18.8	ŀ			8		9 1		103		II			13	H	15	Ħ	17	18	
Angle of Crossings.		ıin	ı	ıin	ı	ı in		ı.	ı in	ı.	ı.	ı ii	ı	ı.	ı	ı	ı.	ı in	
		9	0	9	0	0	0	0	_	9	0	_	0	0	0	0	_	_	
Radius of Curve.																			
	Ē	(1	(4	3	4	53	Ö	À	ŏ	Ŏ	II	12	14	1.5	17	21	25	6	34
'24 MO	is.	6	0	6	0	9	9	•	0	9	0	9	0	•	9	٥	0	0	0
Radius of Inside						56													0
	_	H	_	_				3	4	4	20	9	_	_	∞	2	12	14	11
Heel of Switches. O Nose of Crossing.	I Ps	3	II	∞	44	H	9	9	() 2)4	ΙΙځ	∞	43	- S	10	5	0	Ŋ	103	4
Keel of Switches	표	Ŋ	'n	9	2	œ	∞	6	01	10	11	12	13	13	14	91	17	81	20
. 20 20																			
Heel of Switches to Mose of Crossings						7.													
	Ē	∞ —	_	11	12	.13	14	91	17	<u>∞</u>	19	21	22	23	24	27	29	32	34
Heel of Switches.	Ins.	7.	S	∞	2 42	₹	64 8	6	34	9 }	34	0	43	-165	Ŋ	5 ₽	9	₹ 9	_
Spring of Curve						S													
	_	21																	
Angle of Crossing.		H				1.93													
Anale of Consiser		ı ıı			ı in	ı.	ı in			-		ı E				ı in		ı	
18.8	_				- m	64 80 4										m		ea	
Angle of Crossings.		_	_	_	_	in 2			_	_				_	-				_
														-				-	

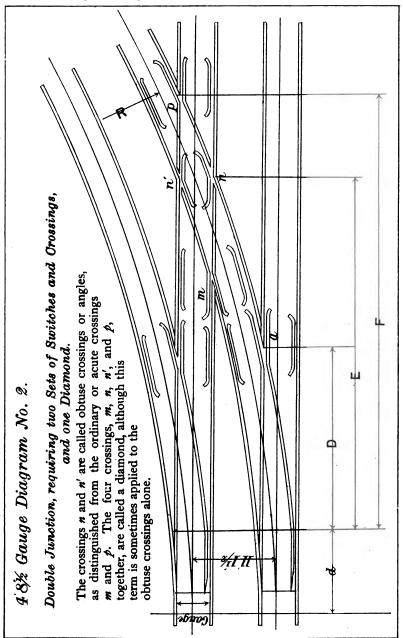


SINGLE JUNCTIONS.	4 ft. 8½ in. Gauge. Table No. 1.
	4 1.

														_						
	Leading of Curver	Ins.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	Redius of Curve.	Ŧ.	٠,		989			941	1037	1139	1244	1355	1470	1590	1844	7112	2409	61/2	3049	
	Trucks clear,	S.	0	0	0	0	0	0	0		0	0		0				0	0	
	Spring of Curve to point where	Ft	78	83	88	94	66	104	109		120	125	130	135	146	156	191	177	188	
	Gauge Lines.	Ins.	∞	43	-	9	9	9	II	∞	4	H	6	9	II	4	6	8	7	
	x Spring of Curve to intersection of Gauge Lines.	Ft	20	75	8	84	8	94	86	103	108	113	111	122	131	141	150	91	169	
	to twose of Crossing.	Ins.	7	0	9	11	4	6	(4	∞	H	9	I	S	3	8	0	II	6	
	D Heel of Switches to Mose of Crossing.	Ft	51	55	220	19	65	89	72	75	79	%	Š	8	96	103	110	116	123	
	to Heel of Switches.	Ins.	9	9	н	2	6	0	4	7	11	3	9	o 1	S	0	∞	3	Ö	
	d Spring of Curve											31								
;	n degrees.	Mins.	38	01	44	22	81	44	92	21	28	46	30	24	9	20	34	22	oi Oi	
	Angle of Crossing.	Ι.	-	7	9	9	9	'n	v	'n		4								
5	.eximu al				- 8 T						III		123		-		-			
	Angle of Crossing.		<u> </u>	ıı			. <u>.</u>		. I	ı	. I	u r	# .	. II II	. <u>=</u>	ı in	i in	.u	ı in	
P		lns.	0	9	9	0	0	9	9	0	0	0	0	0	0	0	0	0	0	0
3	Radius of Curve.			37	47	59	71	84	66	116	133	151	170	161	212	235	285	339	398	461
	to point where Trucks clear,	Ins.		0								0		0	0			0	0	0
	Spring of Curve	Ft	17	80	22	25	28	30	33	36	ထ္တ	41	4	47	49	52	57	62	89	73
•	intersection of Gauge Lines.	Ins.	5/4	01	24	61	103	34	7	II	4	∞	-fs	S	6	I	01	9	8	113
	Spring of Curve to																		9	
	to Mose of Crossing.	Ins.	강	*	9	64 - 4	1 I 💃	2	₽	જ	₹	9	'n	II	∞	'n	0	3	∞ - e	8
	D Heel of Switches	Fi.	12	13	15	11	<u>%</u>	8	22	24	25	27	29	30	32	34	37	41	4,	
	of Switches.	Ins.	1 9	6	ゃ	9	- 	o I	5. 14.	- * I	6	4₹	6	& -∳2	4	0	31	7 2	II	-(a -(a
	b Spring of Curve	Ft.	4	'n	S	9	_	_	∞ —	6	6	ខ្ម	II	I	12	13	14	15	9 <u>1</u>	8
	g. In degrees,	Min.	52	~ 4	4	38	36	54	56	91 (112	14 T	50	4	~	56	24	32	& &	20
	Angle of Crossing.	Deg.	3	~ —	2,	22	2	<u>~</u>	L)	91	5 H	14	E)	12	12	=	ĭ		∞ ₄	~
	stian al																		1 6 <u>3</u>	
	Angle of Crossing.	١.	.≓.	.≒	.≓.	.≓.	. = .	.≓.	Ħ	.≓.	Ξ	.= .	Ξ.	=	Ξ.	Ξ.	Ξ.	≓.	멾.	= -

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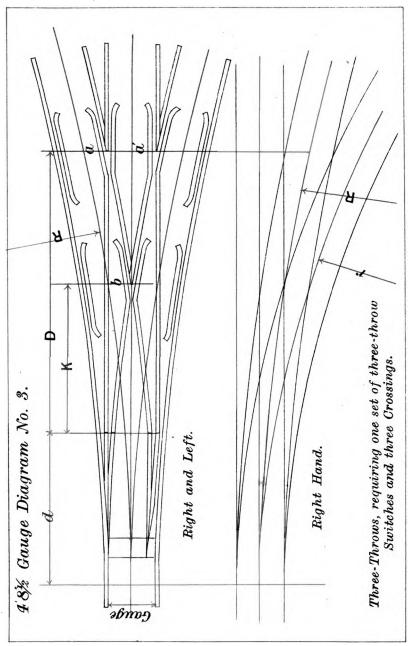
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	Tit. 0/2 in. Gauge. Table No. 2.
Radius of Curve.	F. Ins. 622 0 652 0 680 0 680 0 680 0 941 0 941 0 1135 0 1
Heel of Switches to Mose of Crossing.	Ft. Ins. 109 6 110 6 10 110 6 10 110 6 10 110 110 11
Heel of Switches to Knees of Crossing.	27777 5 5 4 4 5 6 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
Heel of Switches to Mose of Crossing.	Fi. Ins. Fr.
Spring of Curve to Heel of Switches.	F.I.II. 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
Angle of Crossing.	1 in 1 4 4 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
Angle of Crossing.	100 100 100 100 100 100 100 100 100 100
Angle of Crossing.	6.38 6.38
Angle of Crossing.	788 99 00 01 11 21 21 21 21 21 21 21 21 21 21 21 21
Radius of Curve.	FLIns. 32 6 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
F Heel of Switches to Mose of Crossing.	7.28 8.28 24 24 25 25 25 25 25 25 25 25 25 25 25 25 25
E Heel of Switches to Knees of Crossing.	25 25 25 25 25 25 25 25 25 25 25 25 25 2
D Heel of Switches to Nose of Crossing	######################################
Spring of Curve to Heel of Switcher.	子 4 2 2 3 0 4 2 0 0 0 1 1 1 1 1 1 2 1 2 1 2 1 8 1 3 2 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
Angle of Crossing.	11
Angle of Crossing.	1 in 97 1 in 1.97 1 in 1.34 1 in 1.86 1 in 2.80 1 in 2.80 1 in 2.70 1 in 2.70 1 in 3.60 1 in 4.50 1 in 4.5
Angle of Crossing.	111 112 113 113 113 113 113 113 113 113
Angle of Crossing.	11111111111111111111111111111111111111
Angle of Crossing.	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

DOUBLE JUNCTIONS.
4 ft. 84 in. Gauge. Table No. 2.

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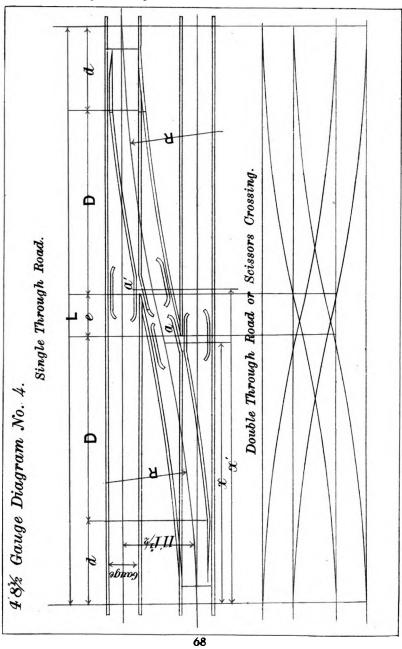


	·	_			
4ft. 8	⅓ in.	Gauge.	Table	No.	3

		Ĕ	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	Radius of Curve.				989														3049	
	Curve,	lns.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	Radius of Inside	F.	265	301	340															
	_ q	ns.	6	01	11	LI	0	0	H	-	N	N	3	4	Ŋ	9	7	∞	6	,
	K Heel of Switches to Mose of Crossing. b				34															
	8 81	ns.	7	0	9	11	4	6	Ø	∞	-	9	11	S	3	0	0	11	6	
	D Heel of Switches to Mose of Crossings.				58															
	Heel of Switches.	ns.	9	01	-	'n	6	0	4	7	11	3	9	01	Ŋ	0	∞	3	0	
ෆ්	b Spring of Curve ot	1	19	20	22	23	24	5 0	27	28	29	31	32	33	36	39	41	4	4	
No.		Γ	62.5	9.9	0.9	5.36	1.4	90.1	1.42	1.17	3.12	3.48	3.84	61.0	<u>68.</u>	2,00	1.31	1.02	2.12	
0	Angle of Crossing.				ii.											_	_	_	_	
Table		-	H	H	8 <u>4 r</u> i	-	1	H	-	H	H	\blacksquare	H	-	<u> </u>	H	-	_	_	
T	Angle of Crossings.							-	TOP		II3		1 12					11 τ		
æ	, and and 30 squar		ï	. . .	ı in	<u> </u>	- 1	=	==	==	==	. I	ī	=	1	=	=	==	. I	
Gauge.		ns.	0	9	9	0	0	9	9	0	0	0	c	0	0	0	٥	0	0	0
65																				
	Radius of Curve.							84	66	116	133	151	170	161	212	235			398	46 I
in.	-	F	29	37	47	59	71	-									285	339		
ft. 8½ in.	Radius of Inside Curve.	Ins. Ft.	6 29	9 37	9 47	6 59	14 9	9	0	0	9	9	0	0	0	0	0 285	0 339	199 0 398	0
8‡ in.	Radius of Inside Curve.	Ft Ins. Ft.	14 6 29	18 9 37	23 9 47	29 6 59	35 6 71	42 6	20 0	58 0	9 99	75 6	85 0	95 0	0 901	0 811	143 0 285	170 0 339	o 661	231 0
ft. 8½ in.	Radius of Inside Curve.	Ins. Ft. Ins. Ft.	5 14 6 29	43 18 9 37	5 23 9 47	5 29 6 59	54 35 6 71	5 42 6	54 50 0	53 58 0	5 <u>1</u> 66 6	53 75 6	6 <u>1</u> 85 o	6½ 95 o	0 901 89	7 . 118 0	73 143 0 285	$7\frac{1}{2}$ 170 0 339	8 I99 o	8 231 0
ft. 8½ in.	Radius of Inside Curve.	Ft. Ins. Ft. Ins. Ft.	7 5 14 6 29	8 43 18 9 37	9 5 23 9 47	To 5 29 6 59	11 54 35 6 71	12 5 42 6	13 54 50 0	14 5½ 58 o	15 51 66 6	16 5\frac{1}{2} 75 6	17 63 85 0	18 61 95 0	0 901 89 61	20 7 118 0	22 73 143 0 285	$ 24 7\frac{1}{3} 170 339$	0 661 8 92	28 81 231 0
ft. 8½ in.	to Nose of Crossings & 8! Real of Switches to Nose of Crossing. Radius of Inside Curve.	Ins. Ft. Ins. Ft. Ins. Ft.	04 7 5 I4 6 29	94 8 44 18 9 37	6 9 5 23 9 47	24 10 5 29 6 59	113 11 54 35 6 71	7 12 5 42 6	4\frac{1}{4} 13 5\frac{1}{4} 50 0	04 14 51 58 0	9 9 15 5 6 6	6 16 54 75 6	$\frac{3}{17}$ $\frac{61}{9}$ 85 o	$11\frac{1}{2}$ 18 $6\frac{1}{8}$ 95 o	0 901 8 6 8	5 20 7 118 0	10 22 71 143 0 285	$3 24 7\frac{1}{2} 170 0 339$	8 26 8 199 o	3 28 81 231 0
ft. 8½ in.	Kadius of Inside Radius of Inside Radius of Inside Curve.	Ins. Ft. Ins. Ft. Ins. Ft.	04 7 5 I4 6 29	94 8 44 18 9 37	6 9 5 23 9 47	24 10 5 29 6 59	113 11 54 35 6 71	7 12 5 42 6	4\frac{1}{4} 13 5\frac{1}{4} 50 0	04 14 51 58 0	9 9 15 5 6 6	6 16 54 75 6	$\frac{3}{17}$ $\frac{61}{9}$ 85 o	$11\frac{1}{2}$ 18 $6\frac{1}{8}$ 95 o	0 901 8 6 8	5 20 7 118 0	10 22 71 143 0 285	$3 24 7\frac{1}{2} 170 0 339$	0 661 8 92	3 28 81 231 0
ft. 8½ in.	Heel of Switches, to Nose of Crossings as at the lot Switches to Nose of Crossing. Heel of Switches to Nose of Crossing.	Ft. Ins. Ft. Ins. Ft. Ins. Ft.	12 04 7 5 14 6 29	13 94 8 44 18 9 37	15 6 9 5 23 9 47	17 24 10 5 29 6 59	18 11 1 5 3 6 71	20 7 12 5 42 6	22 4\frac{1}{4} 13 5\frac{1}{4} 50 0	24 03 14 53 58 0	25 9\frac{1}{2} 15 5\frac{1}{2} 66 6	27 6 16 51 75 6	29 3 17 6½ 85 o	30 II 18 6 1 95 0	32 8 19 64 106 0	34 5 20 7 II8 o	37 IO 22 71 143 0 285	$ 41 \ 3 \ 24 \ 7\frac{1}{8} \ 170 \ 0 \ 339$	44 8 26 8 199 0	48 3 28 8½ 231 0
ft. 8½ in.	Heel of Switches as at the Nose of Crossings K Aleel of Switches to Nose of Crossing. Kadius of Inside Radius of Inside Curve.	Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft.	61 12 04 7 5 14 6 29	24 13 94 8 44 18 9 37	94 15 6 9 5 23 9 47	6 17 2½ 10 5 29 6 59	13 18 113 11 54 35 6 71	10 20 7 12 5 42 6	54 22 44 13 54 50 0	14 24 04 14 54 58 0	9 25 93 15 53 66 6	4 ³ / ₄ 27 6 16 5 ¹ / ₂ 75 6	$0\frac{1}{2}$ 29 3 17 $6\frac{1}{2}$ 85 0	8\frac{1}{2} 30 11\frac{1}{2} 18 6\frac{1}{2} 95 0	4 32 8 19 61 106 0	o 34 5 20 7 II8 o	$3\frac{1}{8}$ 37 10 22 $7\frac{1}{8}$ 143 0 285	$7\frac{1}{8}$ 41 3 24 $7\frac{1}{8}$ 170 0 339	8 26 8 199 o	2\frac{1}{2} 48 3 28 8\frac{1}{2} 231 0
ft. 8½ in.	Spring of Curve to the solution of Switches. Heel of Switches to Nose of Crossings of Switches to Nose of Crossing. Kadius of Inside by Nose of Crossing.	Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft.	4 63 12 03 7 5 14 6 29	5 24 13 94 8 44 18 9 37	5 94 15 6 9 5 23 9 47	6 6 17 2\frac{1}{4} 10 \frac{5}{5} 29 \frac{6}{5} \frac{5}{5}	7 13 18 113 11 54 35 6 71	7 10 20 7 12 5 42 6	8 5\\ 22 4\\ 13 5\\ 50 0	9 13 24 03 14 53 58 0	9 9 25 94 15 54 66 6	10 4\frac{3}{4} 27 6 16 5\frac{1}{2} 75 6	11 $0\frac{1}{2}$ 29 3 17 $6\frac{1}{2}$ 85 0	11 $8\frac{1}{3}$ 30 $11\frac{1}{2}$ 18 $6\frac{1}{3}$ 95 0	12 4 32 8 19 61 106 o	13 0 34 5 20 7 · 118 0	14 $3\frac{1}{8}$ 37 10 22 $7\frac{1}{8}$ 143 0 285	15 7\$ 41 3 24 7\$ 170 0 339	16 II 44 8\frac{1}{8} 26 8 199 0	18 23 48 3 28 83 231 0
ft. 8½ in.	D Spring of Curve to Meel of Switches, D Meel of Switches to Mose of Crossings of Switches to Mose of Crossing. Kadius of Inside D Meel of Switches to Mose of Crossing.	Ft. Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft.	1.21 4 63 12 03 7 5 14 6 29	1.39 5 24 13 94 8 44 18 9 37	1.57 5 93 15 6 9 5 23 9 47	1.75 6 6 17 2½ 10 5 29 6 59	1.93 7 13 18 113 11 54 35 6 71	2.10 7 10 20 7 12 5 42 6	2.28 8 5\frac{1}{4} 22 4\frac{1}{4} 13 5\frac{1}{4} 50 0	2.46 9 14 24 04 14 54 58 0	2.61 9 9 25 94 15 54 66 6	2.82 10 4\frac{3}{4} 27 6 16 5\frac{1}{3} 75 6	3.00 II 0\frac{1}{2} 29 3 17 6\frac{1}{2} 85 0	3.17 II $8\frac{1}{2}$ $30.11\frac{1}{2}$ 18 $6\frac{1}{2}$ 95.0	3.34 I2 4 32 8 19 61 106 0	3.52 13 0 34 5 20 7 118 0	3.88 14 31 37 10 22 71 143 0 285	4.23 15 73 41 3 24 73 170 0 339	4.58 16 11 44 8\frac{1}{8} 26 8 199 0	4.94 18 21 48 3 28 81 231 0
ft. 8½ in.	Depring of Curve theel of Switches. Heel of Switches to Nose of Crossings to Nose of Crossing. Heel of Switches to Nose of Crossing. K	Ft. Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft.	in 1.21 4 63 12 03 7 5 14 6 29	in 1.39 5 24 13 94 8 44 18 9 37	in r.57 5 9\frac{2}{3} 15 6 9 5 23 9 47	in 1.75 6 6 17 24 10 5 29 6 59	in 1.93 7 13 18 113 11 53 35 6 71	in 2.10 7 10 20 7 112 5 42 6	in 2·28 8 5\frac{1}{4} 22 4\frac{1}{4} 13 5\frac{1}{4} 50 0	in 2.46 9 14 24 03 14 53 58 0	in 2.61 9 9 25 93 15 $5\frac{1}{8}$ 66 6	in 2.82 to $4\frac{3}{4}$ 27 6 to $5\frac{1}{3}$ 75 6	in 3.00 II $0^{\frac{1}{2}}$ 29 3 17 $6^{\frac{1}{2}}$ 85 0	in 3 17 II $8\frac{1}{2}$ 30 II $\frac{1}{2}$ 18 $6\frac{1}{2}$ 95 0	in 3.34 12 4 32 8 19 61 106 0	in 3.52 13 0 34 5 20 7 118 0	in 3.88 14 $3\frac{1}{8}$ 37 10 22 $7\frac{1}{8}$ 143 0 285	in 4.23 15 7\$ 41 3 24 7\frac{1}{2} 170 0 339	16 II 44 8\frac{1}{8} 26 8 199 0	in 4'94 18 2\frac{1}{2} 48 3 28 8\frac{1}{2} 231 0
ft. 8½ in.	Angle of Crossing. Spring of Curve Spring of Curve Heel of Switches, to Nose of Crossings Redius of Crossing. K	Ft. Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft.	I in I'21 4 63 12 03 7 5 14 6 29	1 in 1.39 5 24 13 94 8 44 18 9 37	i in r.57 5 94 15 6 9 5 23 9 47	i in 1.75 6 6 17 2\frac{1}{4} 10 \frac{5}{4} 29 \frac{6}{5} 59	1 in 1'93 7 13 18 113 11 53 35 6 71	1 in 2 10 7 10 20 7 12 5 42 6	2 in 2.28 8 5\frac{1}{4} 22 4\frac{1}{4} 13 5\frac{1}{4} 50 0	1 in 2.46 9 14 24 04 14 5 5 5 0	1 in 2.61 9 9 25 93 15 53 66 6	1 in 2.82 to $4\frac{3}{4}$ 27 6 16 $5\frac{1}{3}$ 75 6	1 in 3.00 II $0\frac{1}{2}$ 29 3 17 $6\frac{1}{2}$ 85 0	$ \text{I in 3 17} \text{II } 8\frac{1}{8} \text{30 II} \frac{1}{2} \text{18} 6\frac{1}{8} \text{95 o} $	1 in 3.34 12 4 32 8 19 6 10 0 0	1 in 3.52 13 0 34 5 20 7 118 0	1 in 3.88 14 $3\frac{1}{8}$ 37 10 22 $7\frac{1}{8}$ 143 0 285	$ 1 \text{ in 4.23} 15 7\frac{1}{8} 41 3 24 7\frac{1}{8} 170 0 339$	1 in 4.58 16 11 44 81 26 8 199 0	1 in 4'94 18 23 48 3 28 83 231 0
ft. 8½ in.	Angle of Crossing. Spring of Curve Teel of Switches. Heel of Switches. To Kose of Crossings to Mose of Crossing. Kedius of Inside Radius of Inside	Ft. Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft.	in 13 1 in 1.21 4 63 12 03 7 5 14 6 29	in 2 I in 1.39 5 24 13 94 8 44 18 9 37	in 21 1 in 1.57 5 91 15 6 9 5 23 9 47	in 21 1 in 1.75 6 6 17 24 10 5 29 6 59	in 23 1 in 1'93 7 13 18 113 11 54 35 6 71	in 3 1 in 2 10 10 10 12 5 42 6	in 3\frac{1}{2} 2 in 2.28 8 5\frac{1}{2} 22 4\frac{1}{2} 13 5\frac{1}{2} 50 0	in 3\frac{1}{2} 1 in 2.46 9 1\frac{1}{2} 24 0\frac{2}{2} 14 5\frac{1}{2} 58 0	in 33 1 in 2.61 9 9 25 93 15 5\frac{1}{2} 66 6	in 4 1 in 2.82 10 4\frac{3}{4} 27 6 16 5\frac{1}{3} 75 6	in $4\frac{1}{4}$ 1 in 3.00 11 $0\frac{1}{2}$ 29 3 17 $6\frac{1}{3}$ 85 0	in $4\frac{1}{2}$ 1 in 3 17 11 $8\frac{1}{2}$ 30 11 $\frac{1}{2}$ 18 $6\frac{1}{2}$ 95 0	in 4\frac{3}{4} 1 in 3.34 12 4 32 8 19 6\frac{3}{3} 106 0	in 5 1 in 3.52 13 0 34 5 20 7 118 0	in 5\frac{3}{2} 1 in 3.88 14 3\frac{3}{2} 37 10 22 7\frac{3}{2} 143 0 285	in 6 1 in 4.23 15 7\frac{1}{3} 41 3 24 7\frac{1}{3} 170 0 339	in 4.58 16 11 44 81 26 8 199 0	in 7 1 in 4'94 18 2\frac{1}{2} 48 3 28 8\frac{1}{2} 231 0

THREE THROWS.

48% Gauge Diagram No. 4.



		Redites of Curve.	Ft. Ins. 529 0 600
		Spring of Curve.	Ft. Ins. 153 4 1 1653 4 1 173 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		Spring of Curve to intersection of Gauge Lines at Crossing a!	Ht. Ins. 1882 5 11 1104 7 1 1105 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		Spring of Curve to intersection of Gauge Lines at Crossing &	80 4 1 0 0 2 1 8 4 1 0 0 1 4 0 2 7
		Mose to Mose of. Crossings. 2 2	Fr. Ins. Fr. 111 8 75 8 112 8 8 113 8 75 8 113 2 8 8 114 9 9 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
	4	Heel of Switches to Mose of Crossings. g. g.	111 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
ď	ole No.	Spring of Curve to Switches.	Fr. Ins. Fr. 22 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
ROAD	Table	Angle of Cromings g g!	788 9900111121212141311111 788 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
THROUGH	Gauge.	Radius of Curve.	
THR	ij	Spring of Curve to Spring of Curve.	1. Ins. 1. Ins
	4 ft. 84	Spring of Curve to intersection of Gauge Lines at Crossing a	7. 11. 65. 67. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7
	4.	Spring of Curve to intersection of Cauge Lines at Crossing a	11. 2 2 2 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		Mose to Mose of Crossings.	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
		Heel of Switches to Mose of Crossings.	1. 3 & 2.78 0 a 4 2.7 0 a 4 2.1 4 8 6 0 a 4 2.
		Spring of Curve to Switches.	7. 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		Angle of Crossings.	######################################
		<u> </u>	60

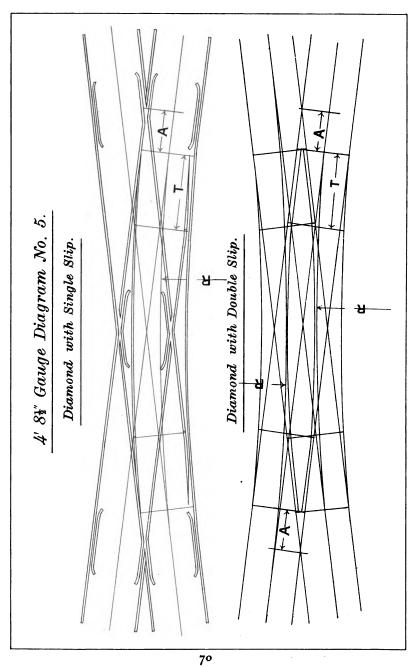


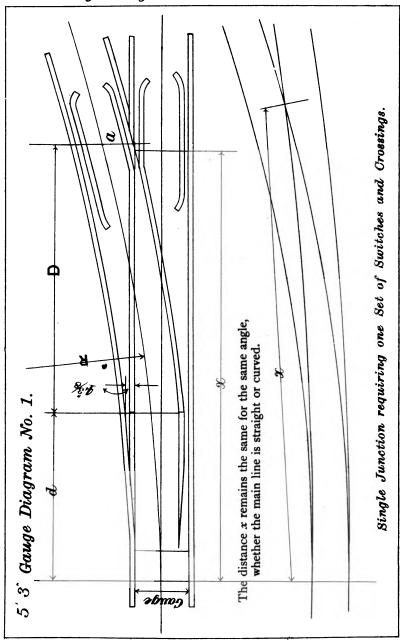
Table No. 5.

DIAMONDS WITH SINGLE AND DOUBLE SLIPS.

4 ft. 81 in. Gauge.

	SINQLE SLIP.									
Angle of Diamond. Radius of Slip.			T Length of Tongue.	Angle of Diamond,	R Maximum Radius of Slip.	Minimum Distance Nose of Crossing to Point of Switch.	T Length of Tongue.			
	Ft. Ins.	ft. Ins.	Ft. Ins		Ft. Ins.	Ft. Ins.	Ft. Ins.			
I in 3	87 6	1 8	6 o	1 in 7	520 O	3 11	12 0			
r in 4	160 o	2 3	7 6	ı in 8	720 0	4 51/2	12 0			
r in 5	260 O	2 9½	9 0	ı in 9	920 0	5 0	12.0			
r in 6	380 0	3 4	9 0	1 in 10	1080 0	5 7	15 0			

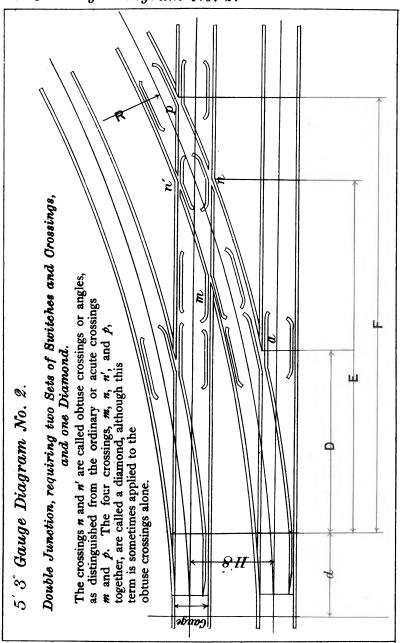
	DOUBLE SLIP.									
Angle of Diamond.			T Length of Tongue.	Angle of Diamond.	R Maximum Radius of Slip.		T Length of Tongue.			
	Ft. Ins.	Ft. Ins.	Ft. Ins.	•	Ft. Ins.	Ft. Ins.	Ft. Ins			
I in 3	77 6	2 11	6 o	1 in 7	460 O	6 10	I2 O			
I in 4	1 50 0	3 11	7 6	ı in 8	640 O	7 9½	I2 O			
I in 5	230 0	4 10½	9 0	I in 9	800 0	8 9	12 0			
ı in 6	360 O	5 10	9 0	I in Io	1000 0	9 9	15 O			



5 ft. 3 in. Gauge. Table No. 1.

		eel of Switches Yose of Crossing.
	1.	pring of Curve to to eel of Switches.
NS.	ble No.	gle of Crossing. g In degrees.
JUNCTIONS	Table	gle of Crossing. 8 In units.
	Gauge.	R addus of Curve.
SINGLE	ft. 3 in.	x Curve to inference to inference of Curve to inference of Curve to Curve t
	9	D leel of Switches Nose of Crossing. 8
		[ee] of Switches.

Control of Control o																				
Consisting of Crossing Consisting Cons	Radius of Curve.	Ins.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Angle of Churre 10 Angle of Course 11 Angle of Course 12 Angle of Course 11 Angle of Course 12 Angle of Course 11 Angle of Course 12 Angle of Course 11 Angle of Course 11 Angle of Course 11 Angle of Course 11 Angle		Ft	591	672	759	851	948	1050	1158	1271	1389	1572	1641	1775	2058	2363	2688	3035	3402	
Angle of Conseing. Angle	in mornagiasiti	Ins.	6	0	3	9	6	0	3	9	6	0	S	9	0	9	0	9	0	
Deg. Min. Ft. Ins. Ft	Spring of Curve to	Ft	78	84	89	94	66	105	110	115	120	126	131	136					189	
Deg. Min. Ft. Ins. Ft	Solve or Crossing.	Ins.	7	5 3	ĸ	3	3	I	0	II	01	∞	7	9	4	1	11	6	7	
Corsing. Angle of Grossing. Angle of Crossing. Angle of Crossing. 28 4 5 5 5 15 7 2 2 0 1 10 8 1 10 0 10 0 0 10 0 10 0 10	D Heel of Switches	Ft	58	62	99	70	74	78	83	85	89	93	97	101	109	111	124	132	140	
Consting. Deg. Min. Ft. Ins. Ft. Ins. Tt. Ins. In Ins. Ins.	01	Ins.	7	0	4	6	-	9	10	8	7	0	4	6	9	8	0	6	9	
Angle of Crossing. Angle of Crossing. Angle of Crossing. 1 28 A 1 5 5 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	p	Ft.	9	22	23	24	56	27	28	30	31	33	34	35	3	41	44	46	49	
Angle of Crossing. Angle of Crossing. Angle of Crossing. 4 Curve 31 52 4 5 5 5 15 15 7 5 15 15 7 5 15 15 15 15 15 15 15 15 15 15 15 15 1	į B	g. Min.	7 38	7 IO	6 44	6 22	7 9	5 44	5 26	5 12	4 58	4 46	4 36	4 24	4	3 50	3 34	3 22	3 10	
Angle of Crossing. 22 8		å	- 01		09	_			-Je		09		-lea	· 						
Angle of Crossing. Angle of Crossing. Angle of Crossing. 1 3 2 4 4 5 5 4 1 1 1 1 1 1 2 6 1 2 1 2 1	12																			
Angle of Crossing. Angle of Crossing. Angle of Crossing. 1 3 2 4 4 5 5 4 1 1 1 1 1 1 2 6 1 2 1 2 1			-	0	9	0	~	~	_	_	_	_	_	_	_	_	^	_	^	
Angle of Crossing. Angle of Crossing. Angle of Crossing. 31 52 4 6 2 17 6 1 1 1 1 1 1 1 2 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 2 1 1 2 1	Radius of Curve.																			
Angle of Crossing. Angle of Crossing. Angle of Crossing. 2 2 2 3 8 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	intersection of Gauge Lines.																			
Angle of Crossing. 2 2 2 2 3 Min. 2 2 3 4 4 5 5 5 9 9 1 13 1 3 2 6 6 10 2 1 14 1 1 1 2 6 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 1	s or evruð de gringg														-					
Angle of Crossing. 2 2 2 2 3 Min. 2 2 3 4 4 5 5 5 9 9 1 13 1 3 2 6 6 10 2 1 14 1 1 1 2 6 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 2 7 1 1 1 1	to Prose of Crossing.	[ns.	₩ **	74	9	61	χ 2/4	5. 14.	S	44	3	64 20 4	7 m	1 3	- e	- No.	13	_	6	
Angle of Crossing. In degrees. S 9 9 4 4 5 2 4 4 5 1 1 1 2 2 6 4 4 5 2 2 4 4 5 1 1 1 1 2 2 6 4 4 5 1 1 1 1 1 2 2 6 1 1 1 1 1 2 2 6 1 1 1 1	Heel of Switches																			
Angle of Crossing. In degrees. S 9 9 4 4 5 2 4 4 5 1 1 1 2 2 6 4 4 5 2 2 4 4 5 1 1 1 1 2 2 6 4 4 5 1 1 1 1 1 2 2 6 1 1 1 1 1 2 2 6 1 1 1 1	01	Ins.	$\frac{9^{\frac{1}{3}}}{8}$	7. 2∖4	81	101	$6\frac{1}{3}$	3	11	$\frac{7}{4}$	$3\frac{1}{8}$	0	∞	43	7	6	I 2	5 3	[0]	3
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	b Spring O Curve																			
	In degrees.	Min.	52	4	4	38	36	54	56	91	12	14	56	9	01	56	24	32	84	01
	Angle of Crossing.	Deg.	31	28	25	61	20	20	17	91	15	14	13	12	12	II	10	0	∞	∞
. estim nl	stinu al																			
P.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B	Angle of Crossing.		ı ib	ı in	ı in	ı ı	ı ıı	ı in	ı ii	ı in	ı E	ı in	ı ii	ı	ı ii	ı ii	ı in	ı in	ı.	. I I

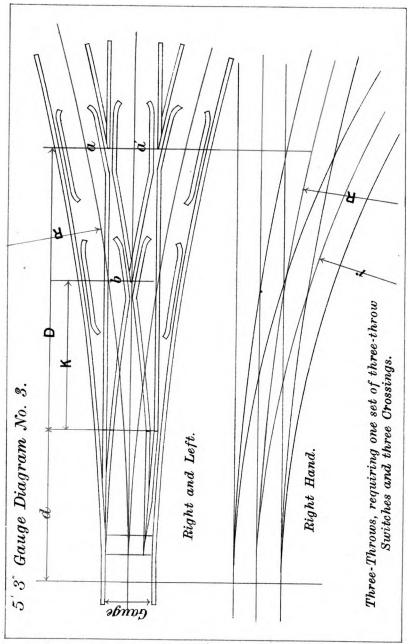


DOUBLE JUNCTIONS. 5 ft. 3 in. Gauge. Table No. 2.

	* 0000000000000000
Radius of Curve.	Ft.Ins. 579 0 579 0 579 0 759 0 851 0 1050 0 1158 0 1175 0 1177 0 1775 0 17
	7 20 20 20 11 1 1 1 1 2 2 2 2 2 2 2 2 2 2
d	8 4 4 20 2 20 1 0 1 4 2 2 2 2 0
Heel of Switches to Mose of Crossing.	1.080420802210217E0
E L	Fr. Ins 5, Fr. Ins 5, 128 2 2 1, 128 4 2 1, 144 6 1, 144 6 1
u'	8 21 40 WOWS 4 KHO 2 4 W4 H
Heel of Switches to Knees of Crossing.	FLIns. 96 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
Hool of Sudicher to	Ft.] 96 96 102 102 123 135 141 154 161 161 161 163 163 163 163 163 163 163
18	× 2
Mose of Crossing.	11 8 8 7 7 7 7 6 7 7 6 7 7 7 8 8 7 9 7 7 7 7 7 7 7 7 7 7 7 7 7
Heel of Switches to	T8228 5 4 4 8 8 8 8 8 9 9 9 9 1 4 2 4 4 5 4
- U	
Heel of Switches.	1 0 1 2 1 2 1 2 1 2 2 2 2 3 3 3 3 3 3 3 3 3
Spring of Curve to	+0 * * * * * * * * * * * * * * * * * * *
, p	F 0 2 2 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	5 440 4 1 8 1 8 4 8 4 8 4 8 4 8 4 8 4 8 4 8 4
d	444NNNN0000 FF000 00
Angle of Crossing.	
1	28.60.85.50.85.48.78.80.40.
in n	NNV000 7 7 7 8 8 8 8 9 0 0 1 1 4
Angle of Crossings.	
1	1200 1 70 4 9 8 8 9 4 4 8 4 8 4 8 4 8 4 8 4 8 4 8
m m	0 7 7 8 8 9 9 9 9 9 11 1 2 E 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Angle of Crossing.	
ĺ	X X X X X X X
1811100010 10 0181111	5,88,9900HH,44,8475F8
Angle of Crossing.	
Radius of Curve.	<u>≅</u> ••••••••••••••••••••••••••••••••••••
ิ ยี " น	Ft.1 32.3 32.4 42.4 79.6 66.6 79.7 111.1 111.1 114.8 116.8 10.8 10.8 10.8 10.8 10.8 10.8 10.8 10
d	1000019019019019019019019019019019019019
Mose of Crossing.	
Heel of Switches to	Ft. 23.33.33.33.33.33.33.33.33.33.33.33.33.3
u u	
Knees of Grossing.	10000000000000000000000000000000000000
Heel of Switches to	l .•
3	7 1 4 4 1 4 4 4 4 4 4 4 6 6 6 6 6 6 6 6 6
8	18 20 0 20 2 4 8 4 4 1 1 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0
Heel of Switches to Mose of Crossing.	
D D	545 333 33 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3
	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
Heel of Switches.	11 0 0 2 4 0 0 0 1 1 7 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Spring of Curve to	
· ·	F 4200 7200 001111222000 00
	8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
Angle of Crossing.	
	108744074100804842
	1 6 8 2 4 9 9 4 4 5 6 9 5 8 4 8 8 8
Angle of Crossing.	HHHHH444444444444444444444444444444444
	H 00 4 10 20 00 00 00 00 00 1 48
	11 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2
Angle of Crossing.	
	28 40 0 28 0 0 40 = 4 2 28 40
	1 1 1 1 2 2 2 2 8 8 8 8 8 9 1 2 2 3 4 8 8 9 9 1 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9
Angle of Crossing.	
, 55	
8	H 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
Angle of Crossing.	
	ниничинины, н.

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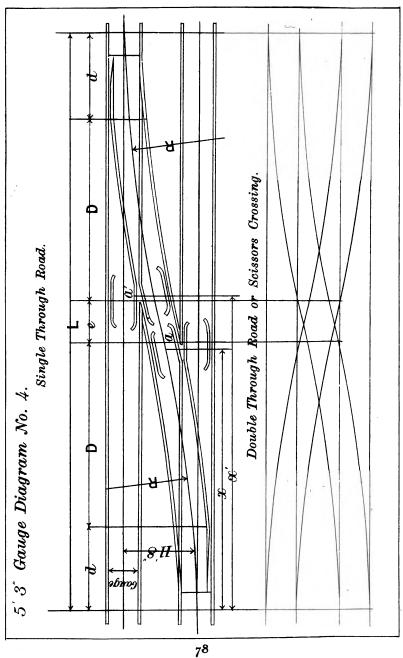
5' 3" Gauge Diagram No. 3.



THREE THROWS. 5 ft. 3 in. Gauge. Table No. 3.

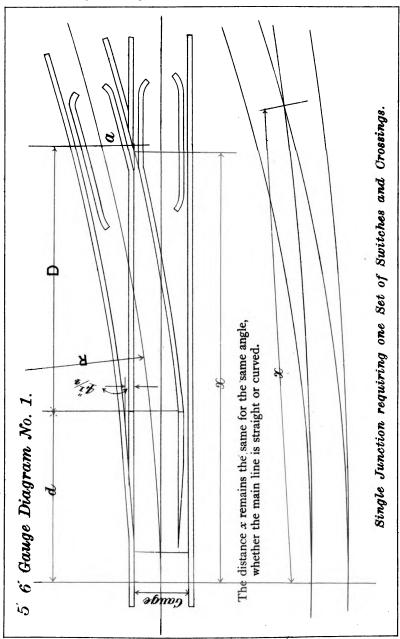
	Ins.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
Radius of Curve.	Ft	16	172	159	351	48	50	58	171	89	172	,4 _I	75	58	93	88	35	03	
	-	-	_	_	20		<u> </u>	Ξ	=	H									
Curve.												0	0				_	_	
apient to suite &														029	182	344	518	701	
a	-33	18	86	8	9	0	8	7	-	8	7	0	4	1	<u> </u>	5 -		<u> </u>	
Heel of Switches to Mose of Crossing.																		34 I	
K																			
to Mose of Crossings. A Ai																			
Heel of Switches	Ft.	58	62	99	70	74	78	82	85	89	93	97	101	60	111	124	132	40	
to Switches, Heel of Switches,	-																		
b paints	Ft																		
a		5.59	2.65	2.00	5.36	2.41	90.2	7.42	11.1	8.12	3.48	3.84	61.6	68.6	9.0	1.31			
Angle of Crossing.															H	달 말.	: ::	ï.	
		-					H	H	=	#	<u>=</u>	H	-	=	<u> </u>	_	=	H	
Angre of Crossings.											Η.	-	-	-	H	=	-	H	
,		Ι	ı I					===	Ξ	Ξ.	H	<u> </u>	Ξ.	H I	<u> </u>	H	
	os.	9	0	9	0	9	9	0	0	٥	0	0	٥	0	0	0	0	0	0
Radius of Curve.																			
	1		_					=	ï	<u> </u>	<u> </u>	<u> </u>	61	(1)	ñ	~	3	4	10
Curve.	Ins.	3	0	6	0	6	9	9	9	0	0	0	0	0	0	0	0	0	0
abiant to suite #	Ft.	91	2 1	56	33	39	47	55	64	74	84	95	20	61	32	59	89	77	28
a	2																		
Heel of Switches to Mose of Crossing.																			
K	_										_								
to Mose of Crossings	Ins.	∞	7.8	9	6 <u>1</u>	5.4	بر دار	Ŋ	44	3	6)4 (3)	2 4 8	4	I P	~¦% O	II	11	6	∞
Heel of Switches																			
		-des	e la		mlæ.	cq			i-e	les				-de		-de	les	rdos.	
Spring of Curve to Heel of Switches,	١.																		
b prime	F	4																	
		1.31	62.1	1.57	1.75	٥.	H	7	3.46	1.64	.82	3.00	3.17	3.34	3.25	\$.88	1.23	1.58	1.64
Angle of Crossing.		E.	E.	E.	<u>.</u>				_			_							
		Ħ	H	-			_	H		_	_								
								-1-	-1-	-		-1-	- les	-		-100		-109	
Angle of Crossings.			in 2																
	Dyring of Curve Heel of Switches, as A. Heel of Switches, as A. Heel of Switches as A. Heel of Switches by Mose of Crossing. Radius of Curve. Radius of Curve. Angle of Crossing. Angle of Crossing. Angle of Switches Angle of Switches Of Switches Heel of Switches. Heel of Switches. Heel of Switches. Angle of Curve. Sal	F. In Spring of Curve. T. In Heel of Switches. T. In Heel of Switches. T. In Kadius of Crossing. T. In Kadius of Crossing. T. In Kadius of Courve. Angle of Crossing. T. Heel of Switches. T. Heel of Switches. T. In Kadius of Curve. Angle of Crossing. T. Heel of Switches. T. In Heel of Switches.	121 121 122 132 133 133 134 135 144 154 155 155	Triangle of Curve By the lot Switches By the l	Constitue Cons	Constitue Cons	Courte C	Constitute Con	Constitue Cons	T. 21 T. 1 S. 1 S. 2 S. 2 S. 2 S. 2 S. 2 S. 2 S	Constitute Con	T.21 F. Ins. Ft. Ins	Current at the case of the cas	Tr. 1	Triangle of Consenings. F. Ins. F. In	Tr. 1	Tried of the control	Tr. 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Tried to the control of the control

5' 3' Gauge Diagram No. 4.



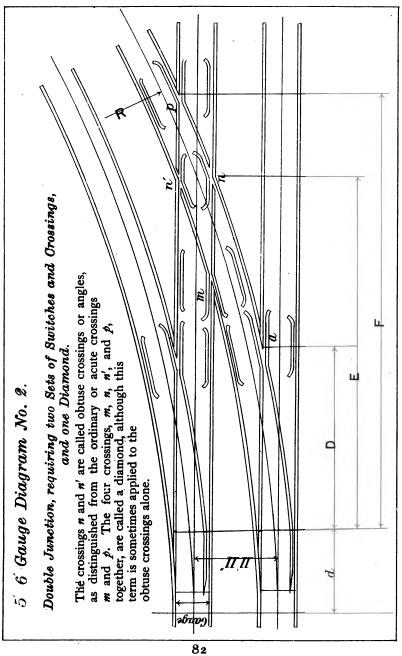
		Radius of Curve.	ğ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
		Я	Ft. 551 (572 573 574 575 575 575 575 575 575 575 575 575
		Spring of Curve to Spring of Curve.	II
		Ť	Ft. 175 176 176 176 176 176 176 176 176 176 176
		intersection of Gauge Lines at Crossing at	II 9778111 97781 8 4 0 8 8
		Spring of Curve to	Rt. 988 988 988 988 988 988 988 988 988 98
		Intersection of Gauge Lines at Crossing a	# 00 00 00 00 00 00 00 00 00 0
		ot avring of Curve to	Ft. 788 899 999 999 999 999 999 999 999 999
		Crossings. 8 &	10 10 10 10 10 10 10 10 10 10 10 10 10 1
		Mose to Mose of	F 7 7 7 8 8 8 8 8 8 8 7 7 7 8 8 8 8 8 7 7 7 8 8 8 8 8 9 9 9 9
	4	to Mose of Crossings.	1 Ins 5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	No.	D Heel of Switches	Ft. 74 4 7 8 8 7 7 7 7 7 7 7 7 7 7 7 7 7 7
๘	A 0	to Heel of Switches.	i
ROAD	Table	b Spring of Curve	7 8 2 2 2 4 3 7 2 8 8 8 E E E E E E E E E E E E E E E E
2	T	Angle of Crossings	7 % % % % % % % % % % % % % % % % % % %
I	ø		2.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B
3	Gauge.	Kadius of Curve.	D. C.
2	ው	Radius of Curve.	Ft. 32 33 34 34 44 4 44 4 44 4 44 4 4 4 4 4
THROUGH	ï	Spring of Curve.	111 111 11 11 11 11 11 11 11 11 11 11 1
•	ft. 3	J Spring S	74.55 442 442 442 442 442 442 442 442 442 4
	5 f	intersection of Gauge Lines at Crossing a	Ins. 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
		os syring of Springs	£1.44.20 88.80 84.44.72.00 87.80 87.
		Intersection of Gauge Lines at Crossing a	108. 17. 17. 18. 19. 19. 19. 19. 19. 19. 19. 19. 19. 19
		ot swing of Curve to	73 1 2 2 2 3 3 4 4 4 4 4 5 3 3 4 5 5 5 5 5 5 5 5 5
		Crossings. R R	8 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		Mose of Mose of	H H H H H H H H H H H H H H H H H H H
		to Mose of Crossings.	08 10 2 2 4 2 4 2 4 2 4 2 4 2 4 2 4 2 4
		Heel of Switches	7. E 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.
		Heel of Switches.	11 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		Spring of Curve	F 4200 288 60 H H I I I I I I I I I I I I I I I I I
		Angle of Crossings.	# XXX XXX XXX X X X
		Angle of Commission	

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5 ft. 6 in. Gauge. Table No. 1.

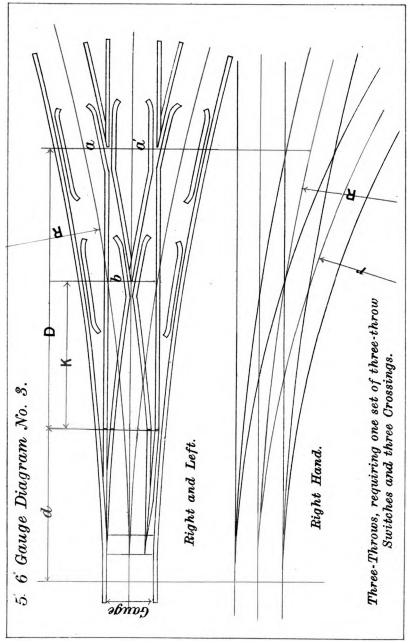
R 1 0 4 C 1 C 0 C H 7 4 0 C	26 26 54
Ft. 619 7049 7049 705 891 1000 1100 1133 1133 1133 1133 1133 11	33 18 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
Therefore of the state of the s	00000
* P	
Some of Crossing.	
G	
Heel of Switches.	
Faunaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaa	38 8 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
N	1 2 3 4 6 6 4
1 1 1 1 2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 6 6 6 6 6
1	24 1 1 2 1 2 1 8 1 8 1 8 1
Z. E.	3.8.8.8.8
Cange Lines. Cang	000000
G G G G G G G G G G G G G G G G G G G	249 275 275 333 396 465 539
Spring of Gurve to the state Lines.	000000
# 2 2 2 2 2 2 8 8 8 4 4 4 4 4 4 4 4 4 4 4	52 52 60 60 71 71
to H H O H I O O O O O O B. S.	4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
G FIFT 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	39 45 45 53 53
T I I I I I I I I I I I I I I I I I I I	a ria riaria
b F 4 NO O V O O O I I I Spring of Curve	50739
нин	13 10 13 10 16 17 18 18 18 18 18 18 18 18 18 18 18 18 18
ii 4 4 8 0 4 9 0 4 4 9 0	2 5 6 13 6 15 10 10 10 10 10 10 10 10 10 10 10 10 10
M	13 13 16 16 16 16 16 16 16 16 16 16 16 16 16



		5 ft. 6 in. Gauge. Table No. 2.
		wi 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	Radius of Curve.	Ft. Ins 704 704 704 705 891 993 1100 1213 1331 1455 1719 1859 1859 1719 1859 1875 3564
	a	70 2700 011 11 11 11 11 11 11 11 11 11 11 11
	d	1. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.
	Heel of Switches to Mose of Crossing.	
	i i	133 133 133 133 150 150 150 150 150 150 150 150 150 150
-	u	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
	Heel of Switches to Kness of Crossing.	1 1 1
	Helj of Emilioper to	Ft. 100 07 07 1113 120 07 1113 120 120 120 120 120 120 120 120 120 120
	8	# 1 THE HELLING O. O. O.
	Mose of Crossing.	1 4 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	D Heel of Switches to	Ft. 79 66 62 10 10 10 10 10 10 10 10 10 10 10 10 10
	Spring of Curve to Heel of Switches.	III 2 5 7 7 1 1 1 1 2 5 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	Ď	7 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		2 4 7 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
	_ d	4440000000000000
	Angle of Crossing.	
		8 47 1 4 5 1 4 8 1 4 8 8 5 1 8 8 7 5 2 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
	'n n	5 2 4 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
%	Angle of Crossings.	
CA		
0		2 4 4 5 7 5 5 5 5 5 5 5 4 7 8 7 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
Z	Angle of Crossing. M	97.7889.0001112222.470
<u>•</u>		2.
Table No.		X X X X X X X
Ig	12	28 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
•	Angle of Crossing.	
		* 000000000000000000000000000000000000
	Radius of Curve.	I
ക്	a	
Gauge.	d	10000000000000000000000000000000000000
B.U	Heel of Switches to Mose of Crossing.	
ð	d and of the state of	Ft. 33 55 74 74 74 74 74 74 74 74 74 74 74 74 74
-:	u	
in.	Knees o Crossing.	11 12 12 12 12 12 12 12 12 12 12 12 12 1
6 in.		11. 7. 1. 7. 0. 2. 0. 2. 2. 2. 4. 1. 0. 7.
6 in.	Heel of Switches to Knees o Crossing.	7. T.
ft. 6 in.	Mose of Crossing. E Heel of Switches to Knees o Crossing.	7. T.
	E Heel of Switches to Knees o Crossing	1 Ins. Ft. I
Ħ.	Mose of Crossing. E Heel of Switches to Knees o Crossing.	Ft. Ins. Ft. In 114 6 22 1 118 8 29 1 1 18 8 29 1 1 18 8 29 1 1 18 8 29 1 1 18 1 18
Ħ.	Heel of Switches to Mose of Crossing. E F Heel of Switches to Knees o Crossing.	1 Ins. Ft. I
Ħ.	Mose of Crossing. E Heel of Switches to Knees o Crossing.	Ins Ft. Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ins. Ins. Ins. Ins. Ins. Ins. Ins
Ħ.	Spring of Curve to Heel of Switches. D Heel of Switches to Mose of Crossing. E E Heel of Switches to Krossing.	Ft. Ins. Ft.
Ħ.	Course to Heel of Switches. Heel of Switches to Mose of Crossing. Heel of Switches to Resent. E	Ins Ft. Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ft. Ins. Ins. Ins. Ins. Ins. Ins. Ins. Ins
Ħ.	Spring of Curve to Heel of Switches. D Heel of Switches to Mose of Crossing. E E Heel of Switches to Krossing.	Ft. Ins Ft. Ins. Ft. Ins. Ft. In in 89 4 10 14 6 22 1 in 1794 5 6 11 20 8 3 29 1 in 1794 6 11 20 8 3 3 2 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Ħ.	Course to Heel of Switches. Heel of Switches to Mose of Crossing. Heel of Switches to Resent. E	Ft. Ins Ft. Ins.
Ħ.	Course to Heel of Switches. Heel of Switches to Mose of Crossing. Heel of Switches to Resent. E	Rt. Ins. Ft. Ins. F
Ħ.	Angle of Crossing. Spring of Curve to Heel of Switches. D Heel of Switches to Nose of Crossing. E E E E E Crossing.	Ft. Ins Ft. Ins Ft. Ins Ft. Ins Ft. Ins It.
Ħ.	Angle of Crossing. Spring of Curve to Spring of Curve to Heel of Switches. D Heel of Switches to Nose of Crossing. E F Heel of Switches to Refere o Crossing.	Ft. Ins Ft. Ins Ft. Ins.
Ħ.	Angle of Crossing. Spring of Curve to Heel of Switches. D Heel of Switches to Mose of Crossing. E E Heel of Switches to Action of Crossing.	
Ħ.	Angle of Crossing. Spring of Curve to Heel of Switches. D Heel of Switches to Mose of Crossing. E E Heel of Switches to Action of Crossing.	Ft. Ins
Ħ.	Angle of Crossing. Angle of Crossing. Angle of Crossing. Spring of Curve to Heel of Switches. D Heel of Switches to Heel of Switches to Refere to Crossing.	Ft. Ins Ft. Ins Ft. Ins Ft. Ins Ft. Ins Ft. Ins
Ħ.	Angle of Crossing. Angle of Crossing. Angle of Crossing. Spring of Curve to Heel of Switches. D Heel of Switches to Heel of Switches to Refere to Crossing.	Ft. Institute Ft. Institut
Ħ.	Angle of Crossing. Angle of Crossing. Angle of Crossing. Spring of Curve to Heel of Switches. D Heel of Switches to Hees of Crossing. Rose of Crossing. Rose of Crossing.	Ft. Ins. Ins. Ins. Ins. Ins. Ins. Ins. Ins
Ħ.	Angle of Crossing. Angle of Crossing. Angle of Crossing. Spring of Curve to Heel of Switches. D Heel of Switches to Heel of Switches to Refere to Crossing.	Ft. Ins Ft. Ins Ft. Ins Ft. Ins Ft. Ins Ft. Ins Ins Ft. Ins
Ħ.	Angle of Crossing. Angle of Crossing. Angle of Crossing. Spring of Curve to Heel of Switches. D Heel of Switches to Hees of Crossing. Rose of Crossing. Rose of Crossing.	Ft. Ins Ft. Ins Ft. Ins Ft. Ins Ft. Ins Ft. Ins
Ħ.	Angle of Crossing. Angle of Crossing. Angle of Crossing. Spring of Curve to Heel of Switches. D Heel of Switches to Hees of Crossing. Rose of Crossing. Rose of Crossing.	Ft. Ins Ft. Ins Ft. Ins Ft. Ins Ft. Ins Ft. Ins Ins Ft. Ins

DOUBLE JUNCTIONS.

2.

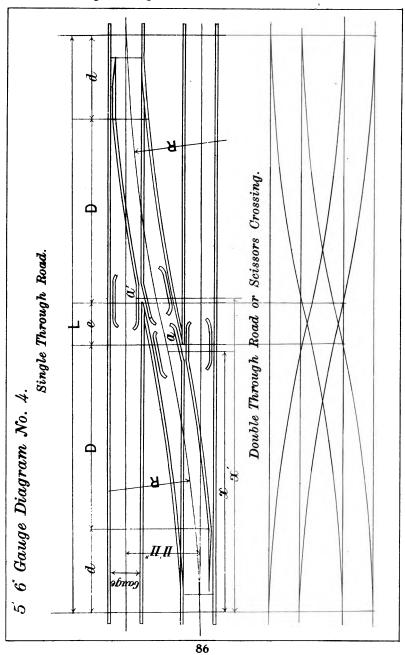


		II .
	Radius of Curve.	Ft. 619 704 704 704 704 704 704 704 704 704 704
	Curve.	# 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	P Radius 10 Inside	Ft. 352 333 335 335 335 335 335 335 335 335
	d de seon or	Ins. 105.
	K Heel of Switches to Mose of Crossing.	7. C 6 4 4 4 4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5
	is a	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	D Heel of Switches to Nose of Crossings.	Ft. 62 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
	Heel of Switches.	III 2 2 4 4 4 4 1 1 1 2 9 2 4 4 1 1 1 1 2 2 4 4 1 1 1 1 1 1 2 2 4 1 1 1 1
	Spring of Curve	F. 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
THREE THROWS. in. Gauge. Table No. 3.		5.29 6.05 6.05 6.75 7.74 7.74 8.12 8.84 8.84 8.12 8.99 9.19 9.19 12.02 11.31
	Angle of Crossing.	
	Angle of Crossings. 8.81	7, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,
Ĭ		B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.B.
Cauge.		ii 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
F &	Radius of Curve.	Ft. 34 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
H 6 ii 6	Cuive,	1 I I I I I I I I I I I I I I I I I I I
柱	abiant lo suibaM	Ft. 171 22 28 34 44 44 45 45 45 45 45 45 45 45 45 45 45
Q	q q	R H 4 7 90 9 80 9 9 9 1 4 0 4 0 4 0 4 0 4 0 4 0 4 0 4 0 4 0 4
	Heel of Switches to Mose of Crossing.	Ft. 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	9 81	品の た8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
	Heel of Switches to Mose of Crossings.	Ft. 144. 144. 144. 144. 144. 144. 144. 14
	Heel of Switches.	I
	Spring of Curve	F 4 20 0 0 0 1 1 1 1 1 2 2 2 8 9 9 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 4 4 4 4
	Angle of Crossing.	

Angle of Crossings. 8 &!

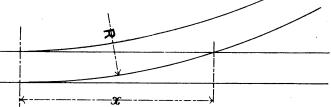
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5' 6' Gauge Diagram No. 4.



			51t, 0 III, Gauge, Table Ite.
		Radius of Curve.	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
			. Ft. 619 704 891 891 100 993 1100 1100 1100 1100 1100 1100
		Spring of Curve to Spring of Curve.	11 1 2 4 2 7 8 8 0 1 1 4 2 7 0 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
			71. 181. 192. 194. 2285. 2217. 2017.
		intersection of Gauge Lines at Crossing 81	81000000000000000000000000000000000000
		Spring of Curve to	Rf. 9888 989 989 989 989 989 989 989 989 9
		intersection of Gauge Lines at Crossing &	g 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
		Spring of Curve to	Ft. 882 883 939 999 999 1115 115 115 115 115 115 115 1
		Crossings. a a!	10 10 10 10 10 10 10 10 10 10 10 10 10 1
		O See of Ose of	F. 13 2 1 1 1 1 1 2 9 9 9 9 9 8 8 8 7 7 7 7 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5
	4	to Mose of Crossings.	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	No.	D Heel of Switches	F1. 662 662 663 74 74 78 78 78 78 78 78 78 78 78 78 78 78 78
4	24	to Heel of Switches,	111 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
ROAD	Table	d Spring of Curve	F 8 2 2 4 2 7 2 6 E E 4 8 8 1 4 4 4
2	H	Angle of Crossings	7,888
I	o)		
9	Gauge.	Radius of Curve.	
THROUGH	ð	aa	Ft. 34 34 34 34 34 34 34 34 34 34 34 34 34
Ē	ä	Spring of Curve to Spring of Curve.	10 10 10 10 10 10 10 10 10 10 10 10 10 1
	9		5 4 4 3 5 5 6 5 7 7 7 7 7 7 7 8 4 3 8 7 7 7 7 7 7 7 8 9 8 9 9 9 9 9 9 9 9 9
	6 ff.	intersection of Gauge Lines at Crossing 81	L X X X X X X X X X X X X X X X X X X X
	-	Spring of Curve to	£ 2 2 2 2 2 2 2 2 2 2 4 2 4 2 4 2 4 2
		intersection of Gauge Lines at Crossing a	13.
		Spring of Curve to	1. 01. 4. 4. 4. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6.
	Crossings. 8 8	al : 480 0 0 0 1 4 7 0 1 0 8 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	
		Nose Mose of	# H = H 4 4 4 4 4 4 7
		Heel of Switches to Mose of Crossings.	II 0 88 88 88 88 88 88 88 88 88 88 88 88 8
			£ 441 8 8 8 4 4 8 9 8 8 8 8 8 8 8 8 8 8 8 8 8
		Heel of Switches.	00 00 00 11 12 12 12 12 12 12 12 12 12 12 12 12
		Spring of Curve	# 42000 000 0 0 0 1 1 1 1 E E E E E E E E E
		18.8	# **** *** *** * * * * * * * * * * * *
		Angle of Crossings.	

Formulæ. Single Turnouts.



A = Angle of Crossing.

G=Gauge of Road.

R=Radius of Curve to Outside Rail.

x =Distance from Spring of Curve to intersection of Gauge Lines.

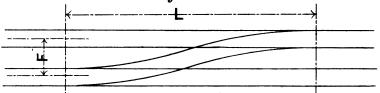
$$A = \sqrt{\frac{R}{2G} - \frac{1}{4}}$$

$$A = \sqrt{\frac{R}{2G} - \frac{1}{4}}$$
 $R = 2G (A^2 + \frac{1}{4})$ $x = 2 AG$.

$$A = \frac{x}{2G}$$

$$A = \frac{x}{2G} \qquad R = \frac{x^2}{2G} + \frac{G}{2}$$

Through Roads.



R = Radius to centre of Road.

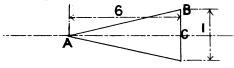
F = Distance, centre to centre of Roads.

L=Distance between springing of Curves.

$$L = 2\sqrt{RF - \frac{F^2}{4}}$$

$$R = \frac{L^2}{4F} + \frac{F}{4}$$

These formulæ apply to angles measured as shown in the following diagram, which represents a 1 in 6 crossing.



The difference between measuring along the side A B, and along the centre A C, except for very obtuse angles (1 in 2 and under), is of no practical importance.

RAIL AT CENTRE, RADI **P** CNA APPROXIMATE VERSED SINE, OR, SET FOR VARIOUS LENGTHS. A Table No. 6.

. ...

FOR VARIOUS LENGTHS, AND KADII.	LENGTH OF RAIL IN FEET.	30	Inches.	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		2.2	Inches.	89
		24	Inches.	0 1 2 4 4 4 5 1 1 1 2 2 1 1 1 2 2 1 1 2 1 1 1 2 1 1 2 1 1 2 1 1 1 2 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1
		2.1	Inches.	2 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
		18	Inches.	
	Radius in Feet			130 175 200 250 300 350 400 450 550 500 1000 1000 3000
	LENGTH OF RAIL IN FEET.	30	Inches.	4 t t t t t t t t t t t t t t t t t t t
		27	Inches.	2 5 0 2 2 2 0 0 2 2 2 0 0 2 2 2 0 0 2 2 2 0 0 2 2 2 0 0 2 2 2 2 0 0 2
		24	Inches.	2 8 3 2 2 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		2 I	Inches.	1 1 2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
		18	Inches.	1
	Radius in Feet.			30 35 40 40 40 40 50 50 60 60 60 70 70 80 80 80 10 10 10

 $\begin{cases} \text{ for 18 feet rails} = 1.5. \\ \text{,, 21 to 24 feet rails} = 1.47. \\ \text{,, 27 to 30 feet rails} = 1.46. \end{cases}$ Value of C

Formula for Versed Sines as above :— $V = \frac{C L^2}{R}$

L=Length of Rail in Feet. R=Radius of Curve in Feet.

V=Versed Sine. C=Constant.

2	
Z OZ	;
Table	

	ge.	s ii.	S ₀	7.2 2.2 2.2 2.2 2.2 2.4 2.4 2.4 2
	5 Ft. 6 In. Gauge.	Speed of Train in Miles per hous,	6	2 11.18 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
28			30	\$12 % chi % chi %
5			8	% % Jana 1 4 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4
VARIOUS			2	4%%×444% ×4%%45%
8	3Ft. o In. Gauge. 3Ft. 338 In. Gauge. 3 Ft. 6 In. Gauge. 4 Ft. 812 In. Gauge. 5 Ft. 3 In. Gauge.	Speed of Train in Miles per hour.	જ	72 2
			-04	91-11-11-11-11-11-11-11-11-11-11-11-11-1
FOR			30	20 4 2 1 1 2 2 4 2 1 1 2 1 2 1 2 1 2 1 2 1
Ĭ			20	4 × × × × × × × × × × × × × × × × × × ×
Ø			01	26 26 26 26 26 26 26 26 26 26 26 26 26 2
CURVES			50	2 2 3 4 5 2 2 3 4 5 2 2 3 4 5 2 3 4 5 2 3 4 5 2 3 5 2 5 2
R	½ In. Gaug	Speed of Train in Miles per hour.	40 5	
2			30 4	20 × 4 × 2
			20 3	20 60 40 4 60 60 80 80 80 80 80 80 80 80 80 80 80 80 80
O	Ft. 8		10 2	2 2 4 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
	4			2.3.3.2.2.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3
RAIL DS.	ıge.	n in ur.	50	1 1 2 5 1 1 1 1 2 5 1 1 1 1 1 1 1 1 1 1
RA DS	Gaı	raii Pou	30 40	33%
	In.	of j		4 6 7 1
TER RA Speeds.	²t. 6	Speed of Train in Miles per hour.	20	2 2 - 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
T S	3 1		2	※ × 2
٥٥	3 Ft. 3% In. Gauge.	i.	50	2.36 1.16
μZ		Speed of Train in Miles per hour.	40	33. - 2 12. - 3 0 12. - 3
ō~			30	25.65 25.65 115.
75			20	7.2 2 4 5 7 5 7 4
SUPER-ELEVATION OF OUTER RADII AND SPEE			2	4.5.2.1.1.1.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2
ER	auge.	Speed of Train in Miles per hour.	50	2.5% 1.3.3 2.3.3 1.3.4 1.3
8			04	"E"E"XX
Ų	in. (30	9日%出了17%
Ā	3 Ft. o I		20	
Ċ.			ខ	まれる。
PE	In. Gauge.	Speed of Train in Miles per hour.	20	H07%
Š			40	46%-4646
			30	72 20 20 20 20 20 20 20 20 20 20 20 20 20
5	.61		20	2 4 1 % 4 5 4 5 1 6 1 7 4 5 1 1 6 1 7 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
5	2 Ft. 6		-01	884 12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
5		Speed of Train in Singles per hour.	20	27 27 11 2 5 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3
TABLE GIVIN	Ft. o In. Gauge.		40 5	40 % TE % PE
֡֝֞֝֟֝֟֝֟֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡			30 4	% % % % % % % % % % % % % % % % % % %
8			20 3	2001-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1
1			10 2	7% 7° 7° 7° 7° 7° 7° 7° 7° 7° 7° 7° 7° 7°
			Ä	2 8 4 70 8 10 11 12 10 8 10 8 10 8 10 8 10 8 10
	Radius of Curve in Feet.			20 90 90 90 10 90 90 90 90 90 90 90 90 90 9